

SL-7-22



RADAR AND TUCKER WAVEMETER DATA
FROM SEA-LAND MCLEAN
VOYAGE 61







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SHIP STRUCTURE COMMITTEE 1978

SL-7-22

TECHNICAL REPORT

on

Project SR-1221

"Correlation and Verification of Wavemeter Data from the SL-7"

RADAR AND TUCKER WAVEMETER DATA FROM SEA-LAND McLEAN

VOYAGE 61

by

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Stevens Institute of Technology

under

Department of the Navy Naval Ship Engineering Center Contract No. NOOO24-74-C-5451

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U. S. Coast Guard Headquarters Washington, D.C. 1978

ABSTRACT

So that more precise correlations between full scale observations and analytical and model results could be carried out, one of the objectives of the instrumentation program for the SL-7 class container ships was the provision of instrumental measures of the wave environment. To this end, two wave meter systems were installed on the S.S. SEA-LAND McLEAN. Raw data was collected from both systems during the second (1973-1974) and third (1974-1975) winter data collecting seasons.

It was the purpose of the present work to reduce this raw data, to develop and implement such corrections as were found necessary and feasible, and to correlate and evaluate the final results from the two wave meters. In carrying out this work it was necessary to at least partly reduce several other channels of recorded data, so that, as a by-product, reduced results were also obtained for midship bending stresses, roll, pitch, and two components of acceleration on the ship's bridge.

As the work progressed it became evident that the volume of documentation required would grow beyond the usual dimensions of a single technical report. For this reason the analyses, the methods, the detailed results, discussions, and conclusions are contained in a series of ten related reports.

This report is one of the six in the series in which the detailed results of the data reduction process are presented. Included in this report is the reduced data from the Third Season Voyage 61.

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INTRODUCTION

It was one of the objectives of the SL-7 full-scale instrumentation program to provide a direct instrumental measure of the wave environment so that more precise correlations could be made between full-scale observations, and analytical and model results. To this end the ship was fitted with a micro-wave radar relative wave meter and various motion sensing devices. A "Tucker Meter" pressure actuated wave height sensing system was also installed.

The purpose of the present project is to reduce and analyze the resulting radar and Tucker meter data obtained on the SEA-LAND McLEAN in the second (1973-1974) and third (1974-1975) winter recording seasons. The purpose of the present report is to present the reduced data from the Third Season Voyage 61.

BACKGROUND

Since the purpose of the present report is only to document a portion of the reduced data, it should be noted that details of the experiments themselves, and of the analyses leading up to the present results, are contained elsewhere. To be specific, References 1 and 2 contain, for both recording seasons in question, a full account of the instrumentation, basic recording, and the nominal circumstances surrounding the present data. References 3 and 5 contain the detail of the reduction of the original data to digital form. Reference 4 contains the detail of the analyses and of the procedures used in generating the present results. Finally, Reference 6 contains the summary, discussion and conclusions.

NOTES ON THE CONTENTS

Each voyage leg was processed, and is presented, as a unit. The first part of the presentation for each voyage leg is a four-part table.

Parts a and b of each table contain the log-book data extracted from Ref. 1 or 2. With the exception of the first column of each page, the meaning of each entry is that established by Teledyne Materials Research. The first column is the run number assigned to each interval during the digitization at D.L. This number is retained for identification throughout.

Part coof each table is a comparison of results from the present digitization with that at TMR. Five columns are stress results obtained at TMR. Stresses are presented in thousands of pounds per square inch. The columns marked 6 through 8 are from the present digitization. Column 6 "range of recorded extremes" was computed from the first pass analysis by scaling the extremes in each interval and subtracting the smallest extreme from the largest. Column 7 is $2\sqrt{2}$ times the process rms. This estimate should compare with the value given by TMR for "rms P to T stress,". Column 8 is the difference of the sample mean of the interval noted, from the sample mean of the first interval digitized in each voyage leg. The remaining columns are various ratios of present results to those obtained by TMR.

Part d of the tables involves indices of the magnitude of <u>raw</u> radar, roll, pitch, vertical and transverse acceleration, and Tucker meter signals. The first index in each case is 4.0 x the rms. The second and third indices are the positive and negative extremes for each channel. The extremes observed for roll and pitch were corrected for electrical zero on tape before scaling. The extremes for all other items were corrected to the sample mean before scaling. The senses of pitch and Tucker meter are not correct for reasons noted in Ref. 4, and it is to be emphasized that all data is raw (uncorrected for anything).

The second part of the presentation for each voyage leg is a series of charts, a pair of charts for each interval. The first of the pair includes plots of spectra of midship vertical bending stress, roll, corrected radar wave elevation, Tucker meter wave, and the mean dynamic head at frame 119. The "mean dynamic head" is a partial correction of the Tucker meter as detailed in Ref. 4. At the left of the first chart is a tabulation of various data; portions of the log book data from the tables, two indices of midship stress, a summary of the magnitude of motions,

and finally a table summarizing wave height statistics obtained from spectra as well as peak-trough analyses of the time histories.

The second chart of the pair for each interval are sample time histories for five of the channels of information treated in the first chart. As noted in Reference 4, there was at the end of data reduction 16-1/2 minutes of valid radar wave elevation data. To produce the charts an 8-1/2 minute portion of this sample was selected.

A fuller discussion of the background and conventions employed in the charts is presented in the Appendix.

REFERENCES

- Wheaton, J.W. and Boentgen, R.R., "Second Season Results from Ship Response Instrumentation Aboard the SL-7 Class Containership S.S. SEA-LAND McLEAN in North Atlantic Service," SL-7-9, 1976, AD-A034162.
- Boentgen, R.R., "Third Season Results from Ship Response Instrumentation Aboard the SL-7 Class Containership S.S. SEA-LAND McLEAN in North Atlantic Service," SL-7-10, 1976, AD-A034175.
- Dalzell, J.F., "Original Radar and Standard Tucker Wavemeter SL-7 Containership Data Reduction and Correlation Sample," SSC-277, SL-7-14. 1978.
- 4. Dalzell, J.F., "Wavemeter Data Reduction Method and Initial Data for the SL-7 Containership," SSC-278, SL-7-15. 1978.
- 5. Dalzell, J.F., "Modified Radar and Standard Tucker Wavemeter SL-7 Containership Data," SSC-279, SL-7-20. 1978.
- 6. Dalzell, J.F., "Results and Evaluation of the SL-7 Containership Radar and Tucker Wavemeter Data," SSC-280, SL-7-23. 1978.

TABLE 1a

SUMMARY OF THR LCG-BOOK DATA CORRESPONDING TO INTERVALS SELECTED FOR WAVE METER DATA REDUCTION (PAGE 1 OF 2)

SEA LAND MC LEAN : 1974-1975 WINTER SEASON : VOYAGE 61 EAST

SEA/AIR TEMP	73/60	70/61	84/48	65/65	66/65	57/54	29/64	58/62	21/16	58/68	56/61	57/61	55/69	56/57	53/58	65/15	53/58	53/54	52/53
DRAFT FT.																			
9 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	121.0	119.1	119.2	118.4	119.0	119.8	119.2			119.5	119.4	82.0	80.9		80.5	80.1	19.4	80.1	79.5
SPEED KT.	29.5	29.0	29.6	28.8	29.62	29.8	29.8	29.1	28.7	29.1	29.1	20.3	19.7	19.8	19.6	19.5	19.5	19.5	19.4
COURSE	281	081	081	081	881	381	381	376	976	376	868	060	262	371	170	871	27.1	071	071
LONGITUDE	64-18 W	64-18 W	64-10 M	64-18 W	64-12 W	64-18 W	49-37 W	49-37 W	49-37 W	49-37 M	49-37 W	49-37 W	36-28 W	36-28 W	36-28 W	26-08 W	8-9	26-00 W	15-42 W
LATITUDE	38-26 N		8-26	8-26	-26	8-2	-26	2	-26	8-26	40-26 N	-2	41-48 N	41-48 N	41-48 N	43-45 N	43-45 N	43-45 N	46-12 N
CAT	28	9	23	6 9	6 9	28	22	09	20	07	25	8 6	69	42	8 8	69	2483	86	09
DATE	-01	-01	-01	83-81-75	- 02	-02	-02	-02	- 82	-02	-03	- 63	-33	- 63	-84	-34	83-34-75	-05	-05
INT N	18	54	28	33	36	66	41	14	51	53	57	-	6	17	52	33	41	64	57
INDX NO.	r	9	7	80	5	13	11	12	13	14	15	16	18	20	22	54	56	28	30
TAPE NO.	223	223	223	223	223	223	223	223	223	223	223	225	225	225	225	225	225	225	225
A RUN	2518	2524	2528	2530	2536	5539	2541	2547	2551	2553	2557	2621	5689	2617	2625	2633	2641	5649	2657

TABLE 15

SUMMARY OF TMR LCG-800K DATA CORRESPONDING TO INTERVALS SELECTED FOR WAVE METER DATA REDUCTION (PAGE 2 OF 2)

SFA LAND MC LEAN : 1974-1975 WINTER SEASON : VOYAGE 61 FAST

		THE LOG-BOOK COMMENTS		ROLLING 18 DEG PORT 5 STR		,	/ HEAVY ROLL		HEAVY ROLL												
		VISUAL MEATHER	DCAST /	PAIN FOG / ROL	RAIN /	PAIN LIGHTNING	RAIN LIGHTNING	DCAST /	CAST / SLOW	DCAST /		DCAST /	PT CLDY /	PT CLDY /	CLEAR /	CLEAR /	OCAST /	FOG OCAST /	FOG RAIN /	FUG RAIN /	FIG RAIN /
<-SWELL->	HT LENGTH	FT. FT.	3 688		8 628	8 623	9	9	9	00	80	00	9	663	623	683	683	683		2 828	2 822
PFL	SWELL	DIR	1445	1445	566	566	566	506	566	1495	1495	1495	1495	1575	1465	1590	159P	1599	1599	1590	1315
MAVE	HT.	FT.	~	7	9	9	•	7	7	5	7	7	•	~	-	-	-	-	-	•	
REL	MAVE	018	1445	1215	885	888	566	545	566	1265	1495	1779	1695	1575	180	1599	159P	1590	1599	1590	1315
CREL WINDS	DIRISPEED	/(KT)	1445/15	1215/38	885/35	885/43	07/566	545/25	52/566	1265/25	1495/18	1779/15	51/5691	1575/25	182 /10	1599/15	1599/15	1599/18	1599/19	1598/ 5	1315/15
Ĭ	SEA	STATE	4	1	œ	0	00	9	9	9	3	1	7	9	3	4	1	0	3	7	7
0.1.	Z O X	DN	2518	2524	2528	2537	2536	2539	2541	2547	1550	2553	1557	2601	5689	2617	2625	2633	2641	5649	2657

COMPARISON OF THE RESULTS FOR MIDSHIP VERTICAL BENDING STRESS WITH CORRESPONDING RAW DIGITIZATION RESULTS AT DAVIDSON LABORATORY

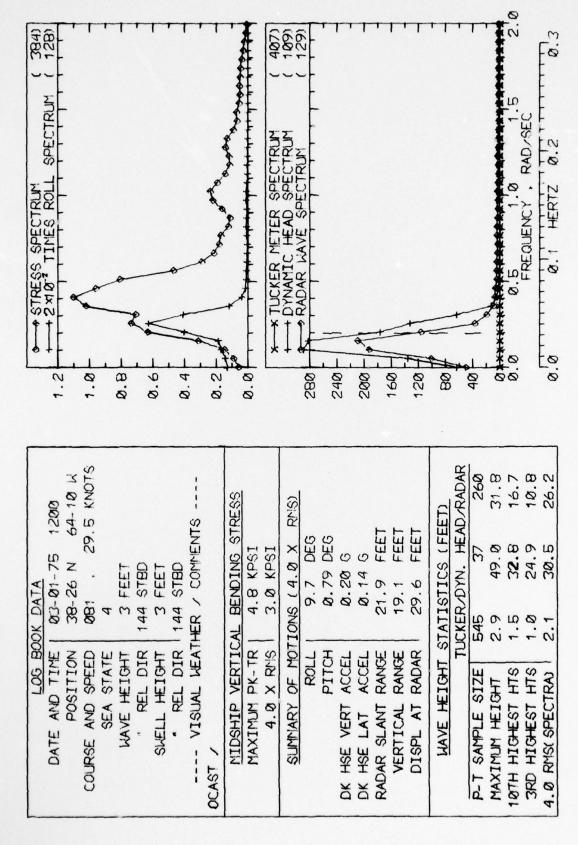
SEA LAND MC LEAN : 1974-1975 WINTER SEASON : VOYAGE 61 EAST

* <column ratios=""></column>		(9)	,	(3)			1,06	1.22	1.25	1.38	1.81	1.29	1.36	1.22	0.92	1.17	1.21	1.11	1.11	36.0	1.05	1.33	1.14	1.01	4.22
IMN RAT		(9)	`	(3+2)			9.84	85.0	•	1.13	•	•	1.89	•		1.05	1.86	•	1.11	06.0	•	•		1.91	
corr			•				. 2	1.05	0	9.		-	1.14	0		3	0	0	96.0	0	-	8	6.	1.06	1.04
*	*	4	\$ 5	•	*	4	*	4	•	*	4	4	4	4	4	*	4	4	4	4	•	4	4	4	4
NDI	REL	A	STRES	S	æ		0.57	6.67	. 3			9.	8.25	-:	E.		6			•	9	1.48	2.03	1.89	1.81
DIGITIZAT	2.83X	SAMPLE	RMS)	KPSI	(7)			3.15	4.			-	3.01	•	•	•		•	3.27	•	•	•	•		5.19
7.	ANGE	ECORDE	2	in	0		-	8.23	•		7.67	8.53	•	8.51	10.50	85.6		-	8.37	3	.3	5.48	4.	4.85	21.02 ***
*	*	*	*	4	4	4	4	4	4	4	*	4	4	4	*	*	*	45	ü	*	*	*	*	4	4
î	MAX 1ST	00	STRESS	ISd	(5)		1.30	1.56	O	1.28	-	1.27	1.37	.2	-	6.	0	G	2.60	.2		2	2.	.0	2.
	528	-10	STRESS	KPSI	(4)		1.99	3.01	3.37	2.81	2.11	2.77	2.63	3.16	3.97	4.17	3.65	3.93	3.46	3.25	2.89	2.47	2.45	2.19	2.10
RESULTS-	MAX	10	STRESS	A	(3)		0	6.87	9	5.75	4.23	6.63	•	•	11.41	•	•		7.54	•	•	4.12		4.81	•
- ;	NO.	ST	MODE	BURSTS	(2)		11	32	35	34	41	56	17	6	14	2	7	0	0	0	6	0	0	6	6
>	. ON	A	CE	X	(1)		106	160	9.5	16	9	122	-	96	7.6	19	76	74	76	8 9	86	75	73	26	73
4	4	•	*	4	4	4		4	*		4		*		•	4		4	*		*		*		4
		0.1.	RUN	. DN			2518	2524	2528	2530	2536	2539	2541	2547	2551	2553	2557	2601	2629	2617	2625	2633	2641	5649	2657

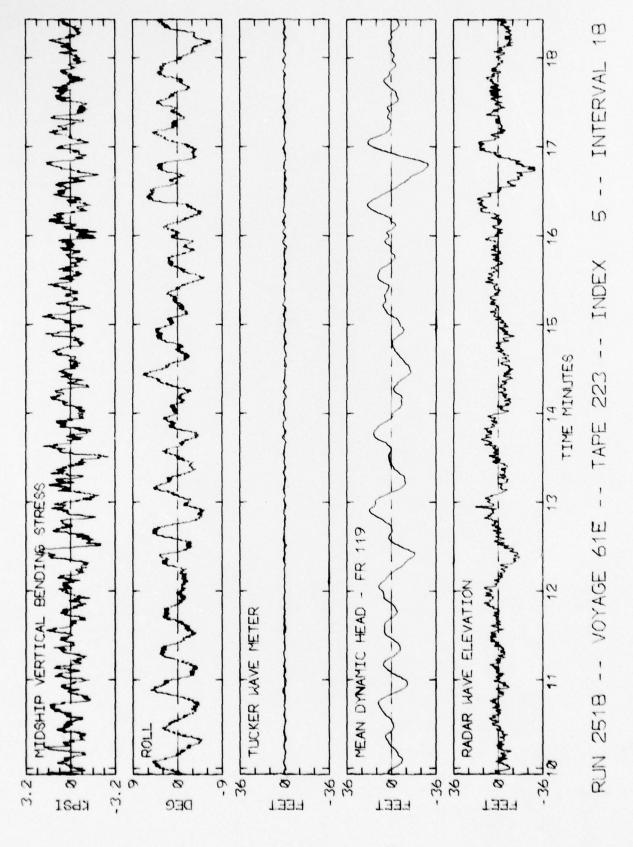
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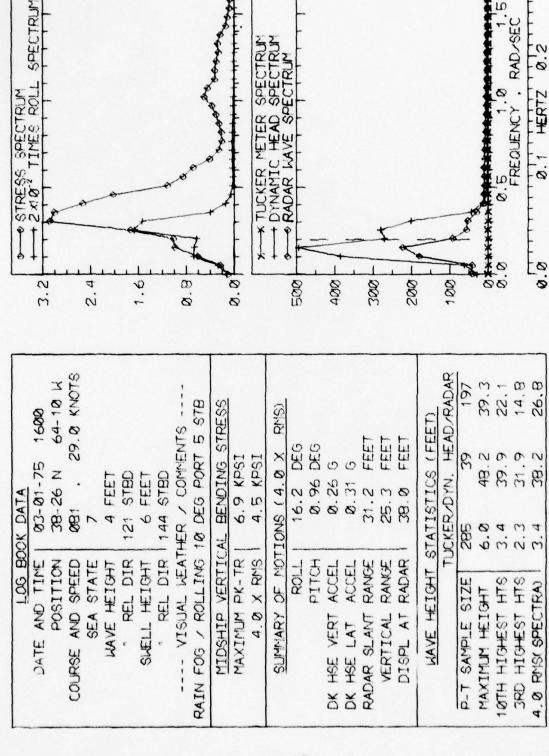
SUMMARY OF RAW DIGITIZATION RESULTS FOR RADAR RANGE ROLL, PITCH, DECK HOUSE ACCFLERATIONS, AND TUCKER METER

	ROED		4444	44446000000
	CKER RECD EXTR	2 6 6 6	w 1 1 w	4 m m m m n n n n n - n
	4.8 (RMS)	~ m m 3		40004000000
51	EL>< DRDED REMES (G)	6.2	2225	
61 EA	ACCE RECO EXTR	86.3	22.20	444600000000
	4.8 (RMS)	3.31 3.31 3.32 3.38	4002	~4~~~~~~~~
	ROED ROED EMES (G)	2 8 8 8 8	6669	200000000000 2000000000000000000000000
EASON	RECOR	2 5 5 5 5		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
75 WINTER SEASON : VOYAGE	4.8 (RMS)	3.28 8.26 9.32 8.28	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
S WINTE	ROED FMES DEG	1.5	-1.8	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
0	RECO EXTR DEG	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	9 2 9 9 9	
AN : 1974-1	4.8 (RMS)	1.6	2.000	000000000000
	RDED EMES DEG	11.1.	-15. -16. -24.	
) ¥	RECOR EXTRE DEG	w 20 m n		m - r 0 1 2 r 0 1 1 7 7
A LAND	4.8 (RMS)	2000	0 1 1 m	2221 2221 2474 2782 2787 2787 2787 2787
SE	RDED EMES	-29. -43. -23.	-30. -22. -23.	249. 246. 236. 236. 237. 237. 218.
	ADAR RECO EXTR	2000-		
	(8 K S)	22. 31. 32.	31.	24 4 6 2 2 4 4 6 2 4 6 2 4 6 2 6 2 6 2 6
	Port.	2518 2524 2528 2538	2536 2539 2541 2547	2551 2553 2553 2553 2689 2617 2675 2641



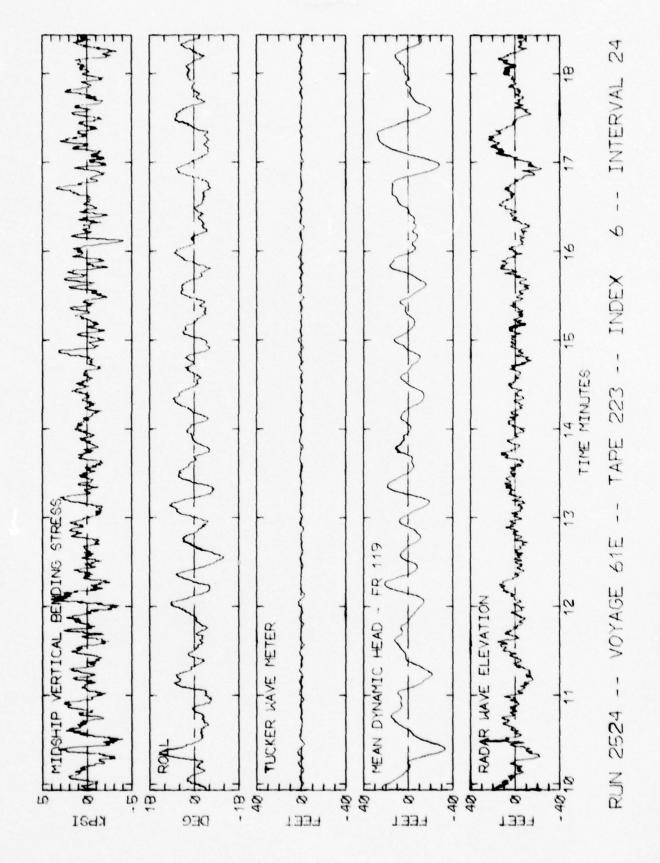
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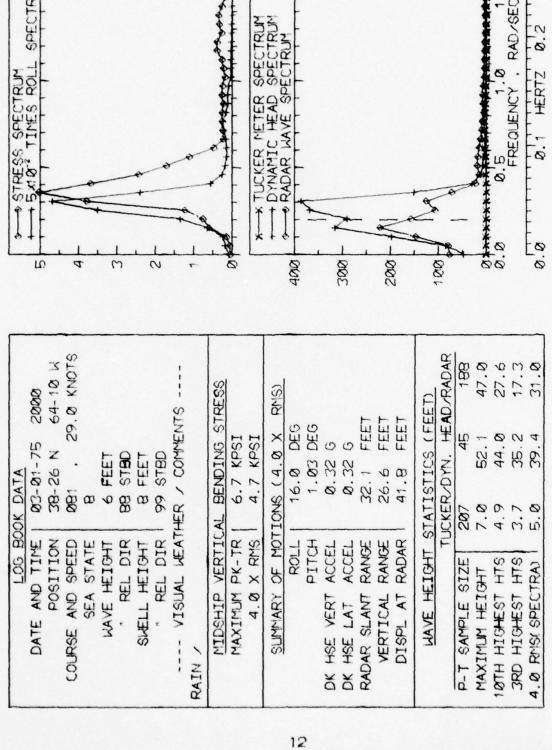




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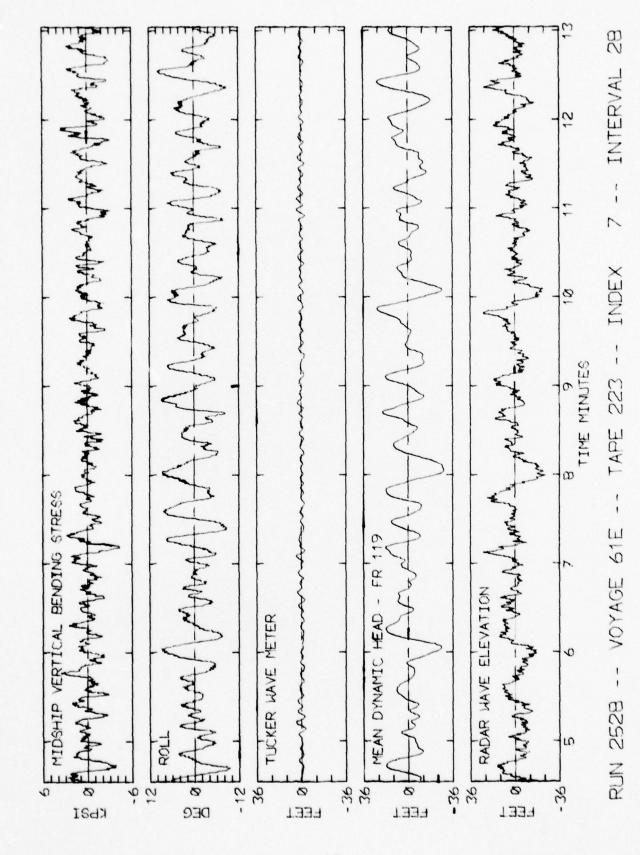
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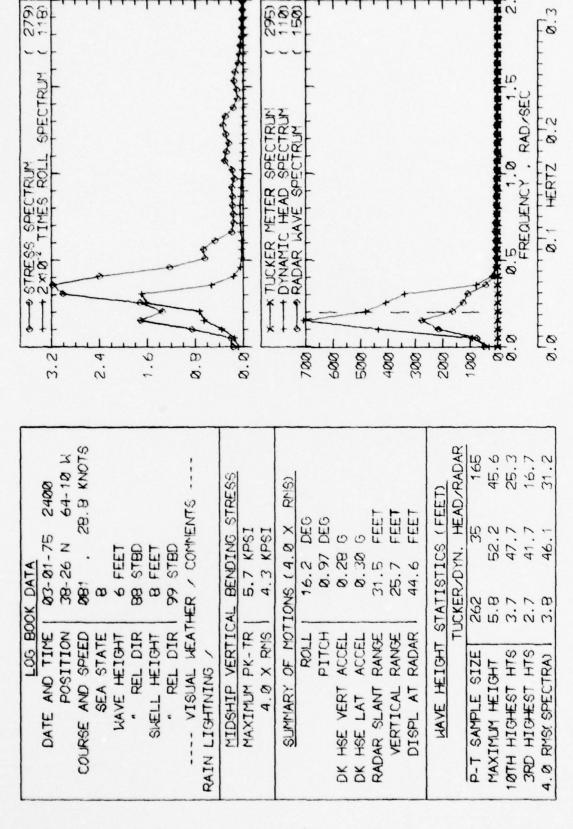




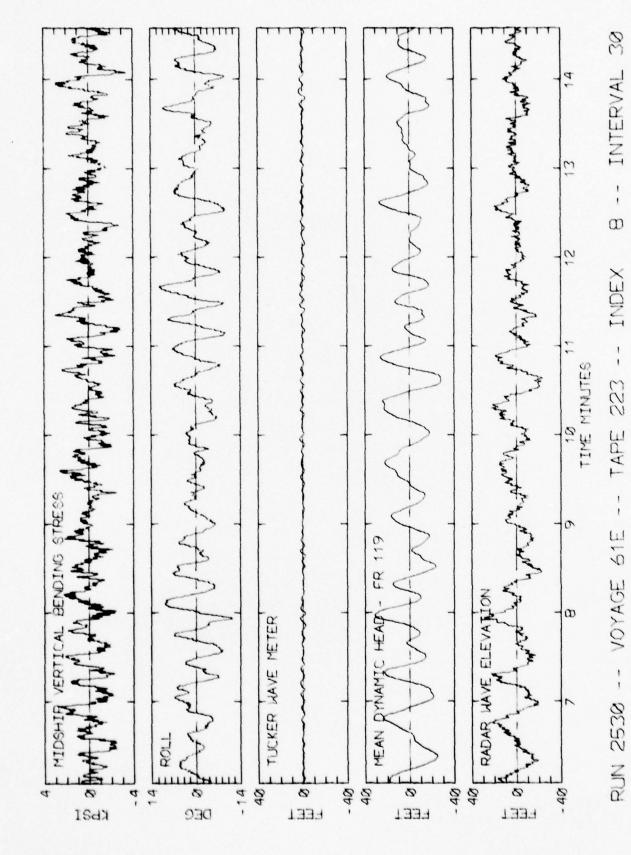
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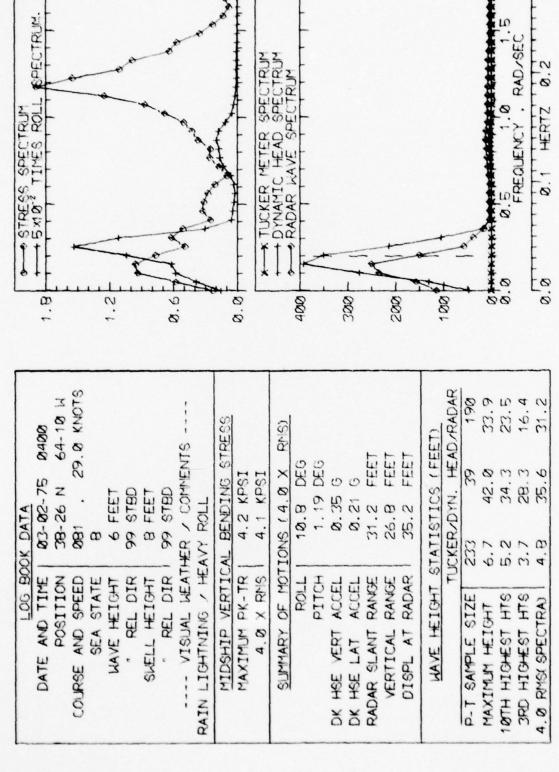
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30 INTERVAL 0 INDEX 223 TAPE 1 61E VOYAGE RUN 2530 --

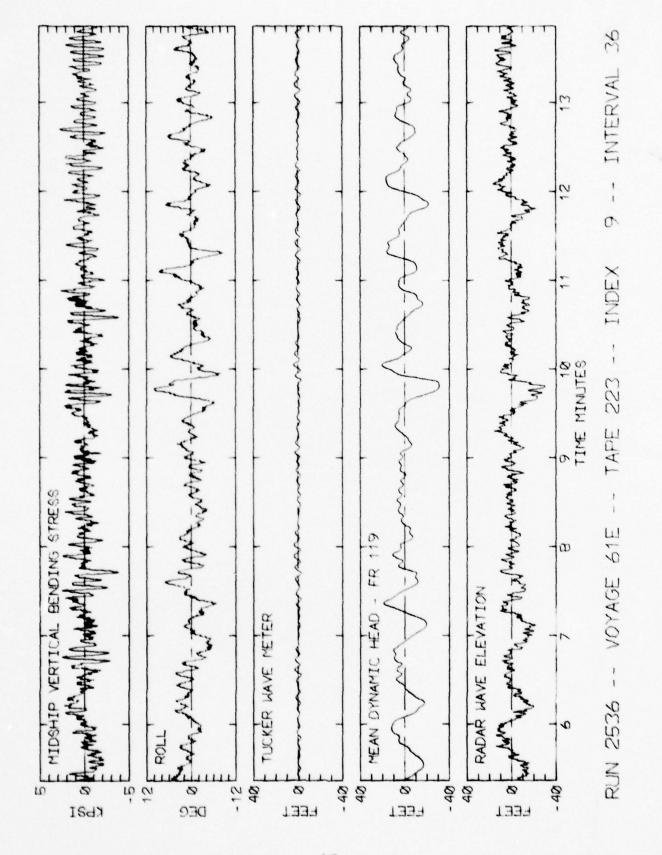


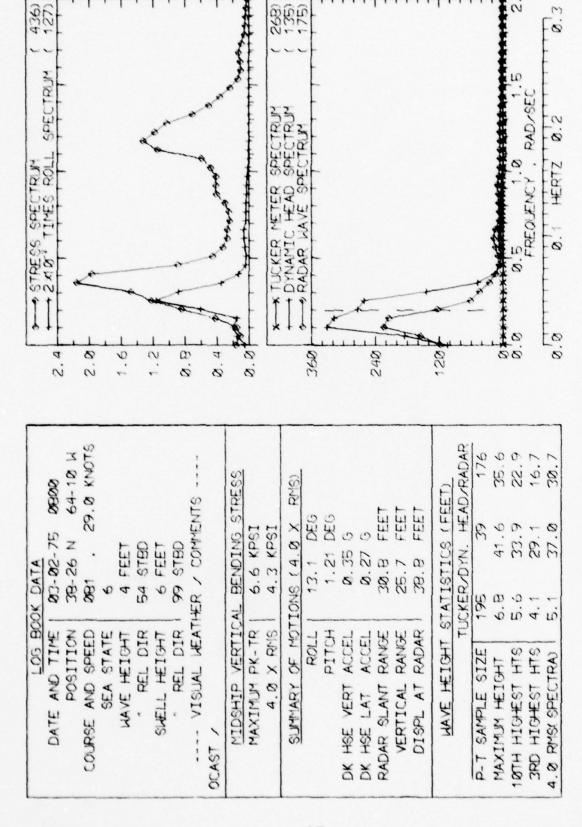


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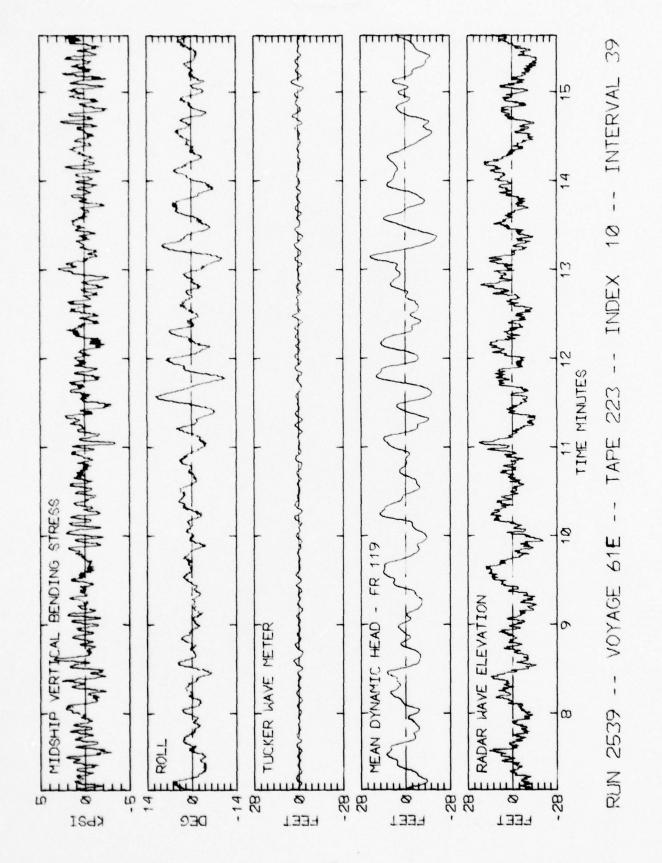
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36 INTERVAL -- 6 INDEX 223 --TAPE VOYAGE 61E RUN 2536 --



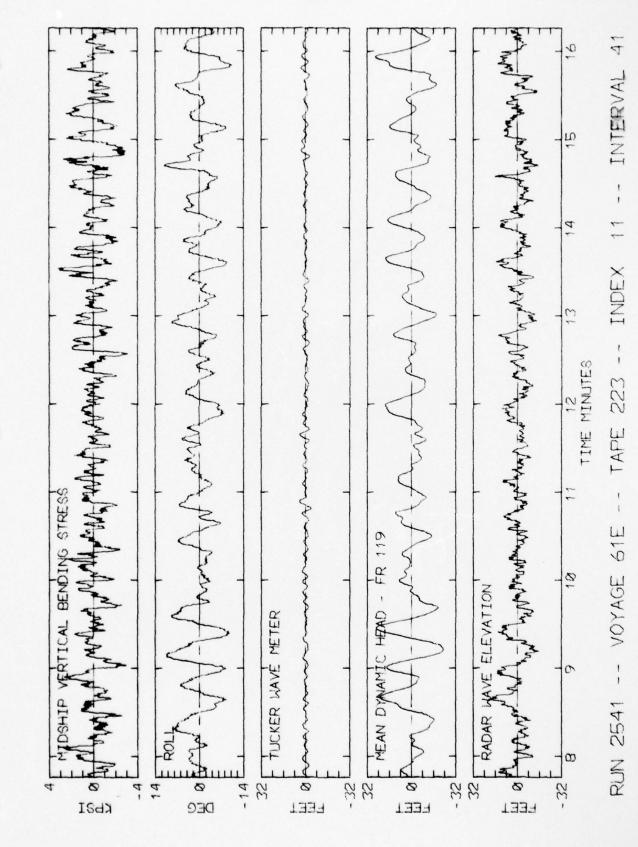


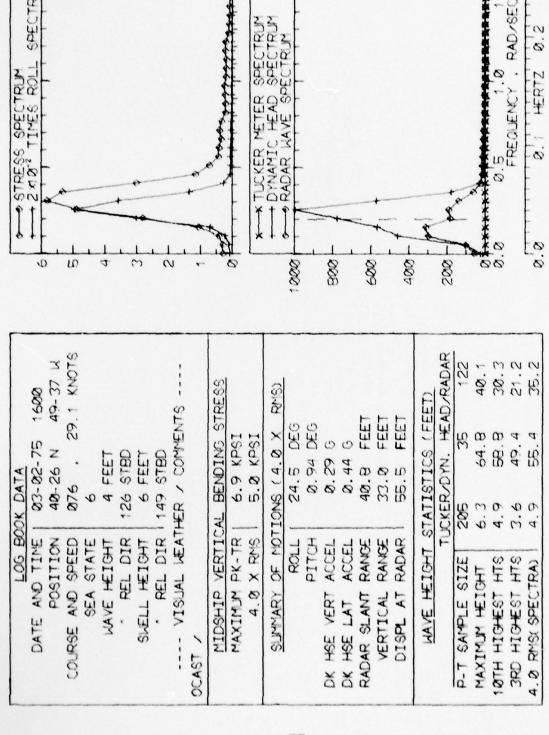
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OOK DATA	DATE AND TIME 83-82-75 1288 POSITION 48-26 N 49-37 W	COURSE AND SPEED 881 , 29.8 KNOTS			* REL DIR 99 STBD	SWELL HEIGHT 6 FEET	_	VISUAL WEATHER / COMMENTS	OCAST / SLOW HEAVY ROLL	MIDSHIP VERTICAL BENDING STRESS	1	4.0 X RNS 4.2 KPSI	SUMMARY OF MOTIONS (4.0 X RMS)	ROLL 15.0 DEG	PITCH 1.05 DEG	DK HSE VERT ACCEL 0.32 6	DK HSE LAT ACCEL 0.28 G	RADAR SLANT RANGE 31.1 FEET	VERTICAL RANGE 26.3 FEET	DISPL AT RADAR 37.5 FEET	WAVE HEIGHT STATISTICS (FEET)	TUCKER/DYN, HEAD/RADAR	P-T SAMPLE SIZE 249 41 206	MAXIMUM HEIGHT 6.8 44.4 32.7	50	3RD HIGHEST HTS 3.2 32.5 14.4	

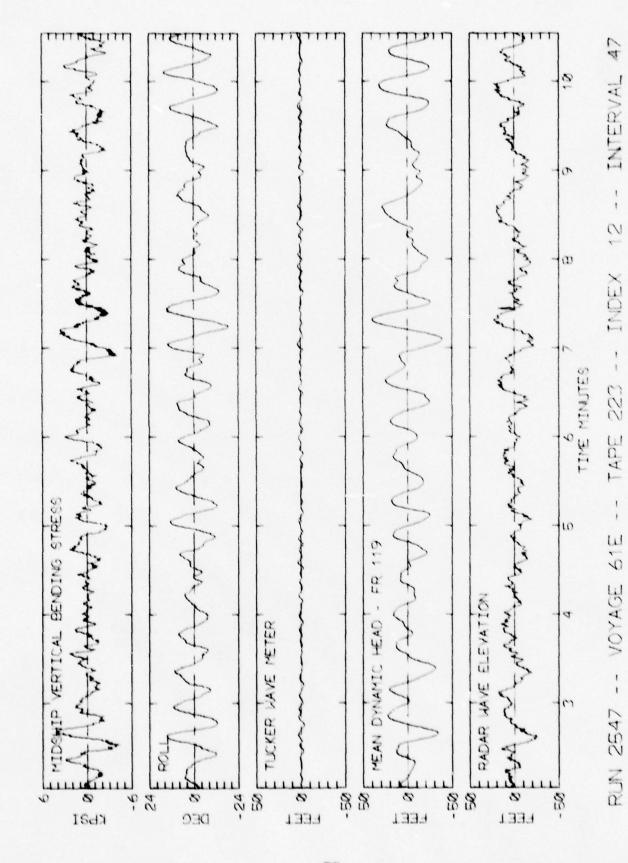
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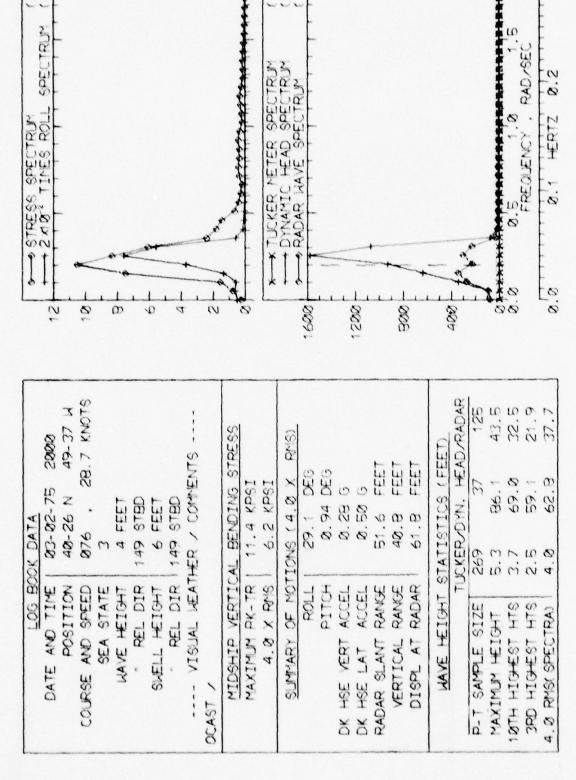




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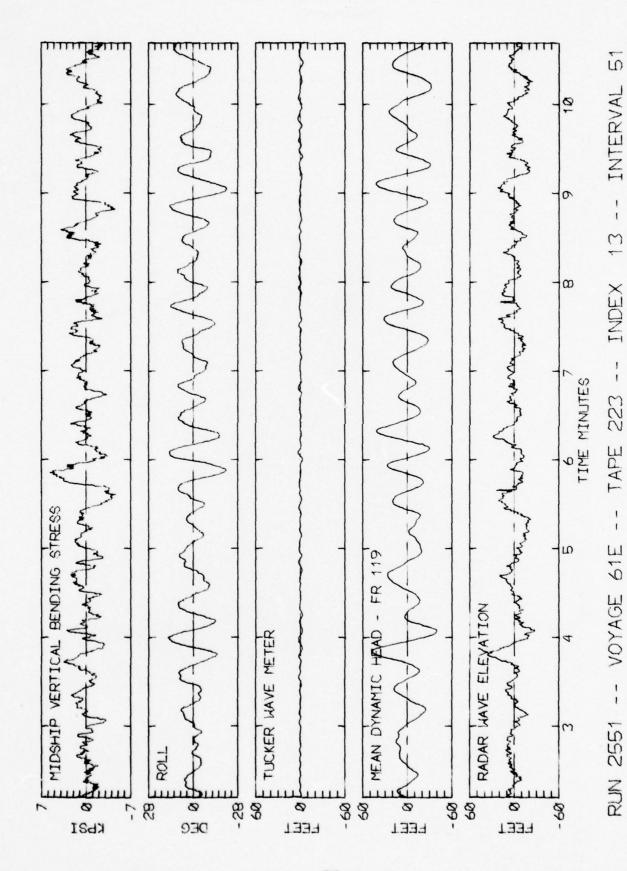


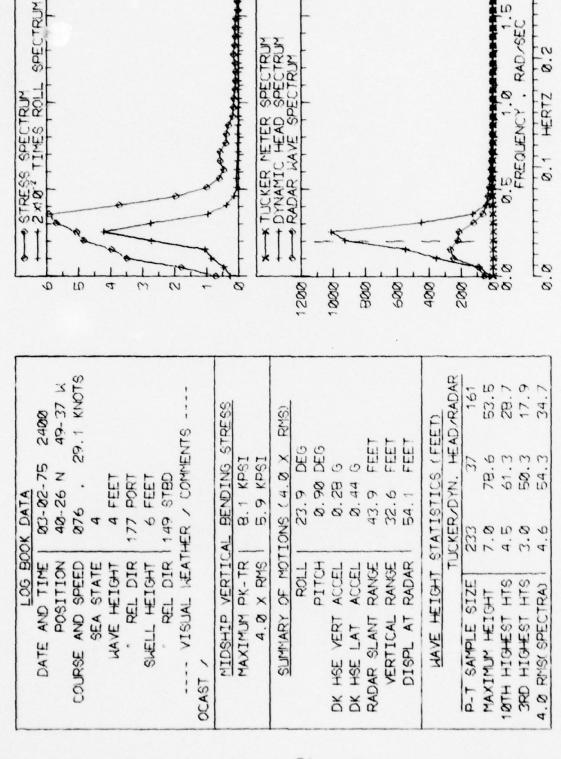


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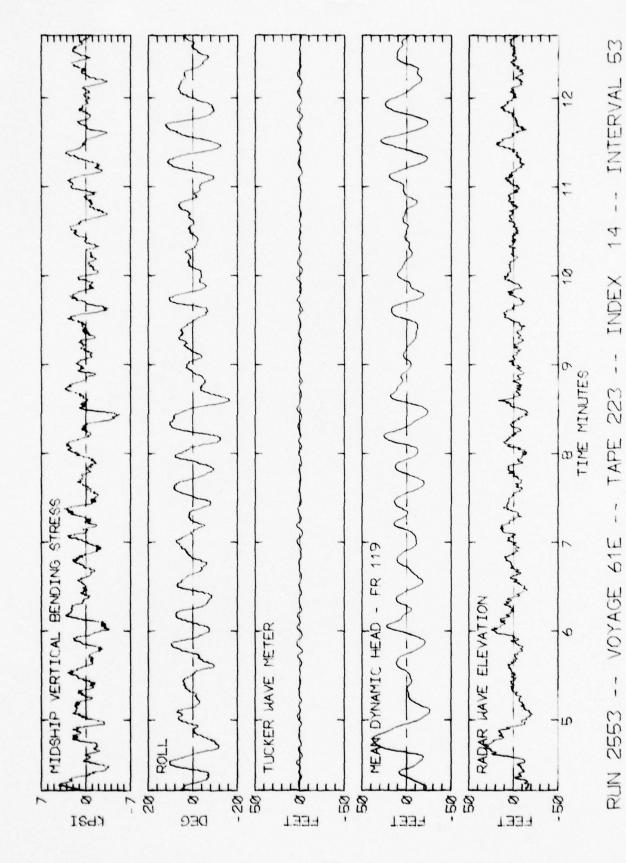
C)

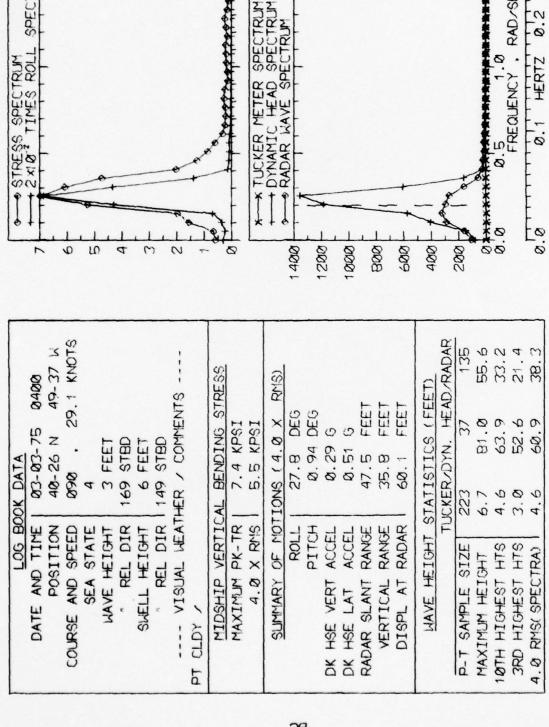
in INTERVAL 13 --INDEX 223 TAPE 61E VOYAGE RUN 2551





23 INTERVAL 14 --INDEX 223 --TAPE 61E VOYAGE RUN 2553 --





38.38

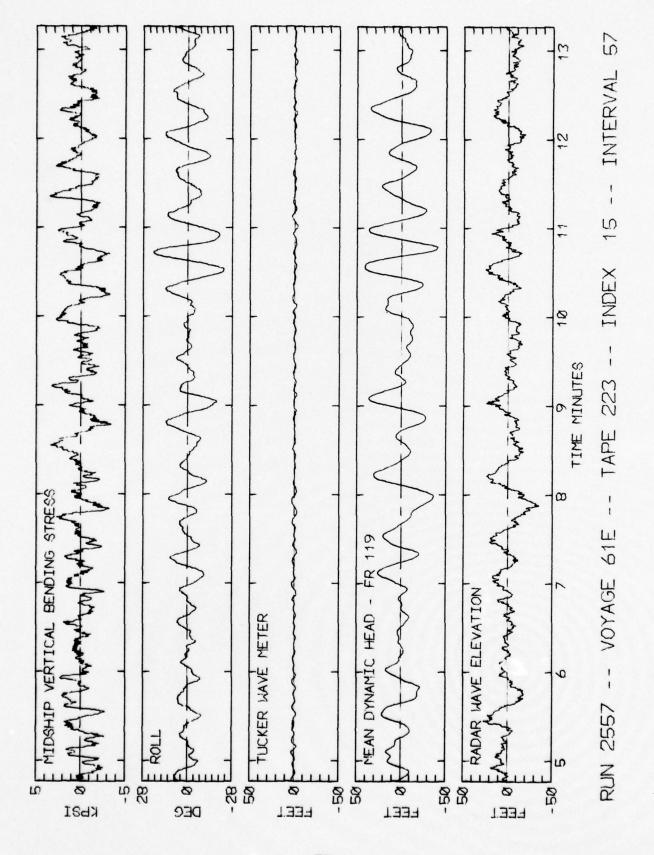
58

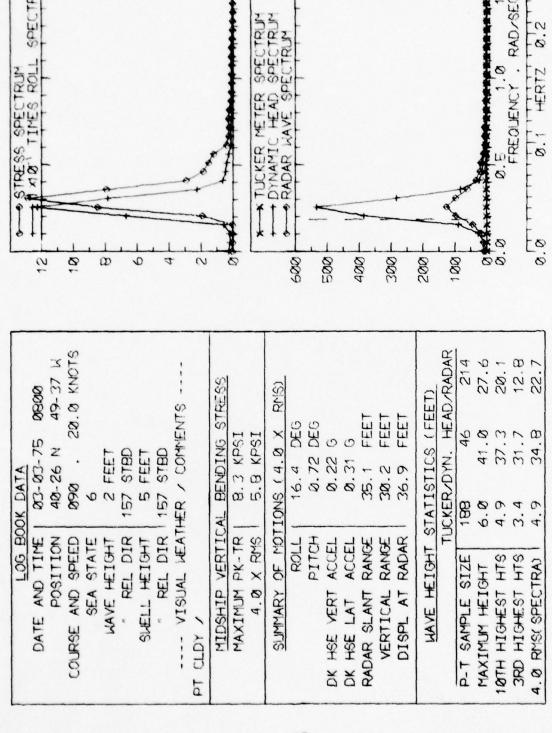
SPECTRIM

57 INTERVAL 15 --TAPE 223 -- INDEX ! RUN 2557 -- VOYAGE 61E

6.3

. RAD/SEC



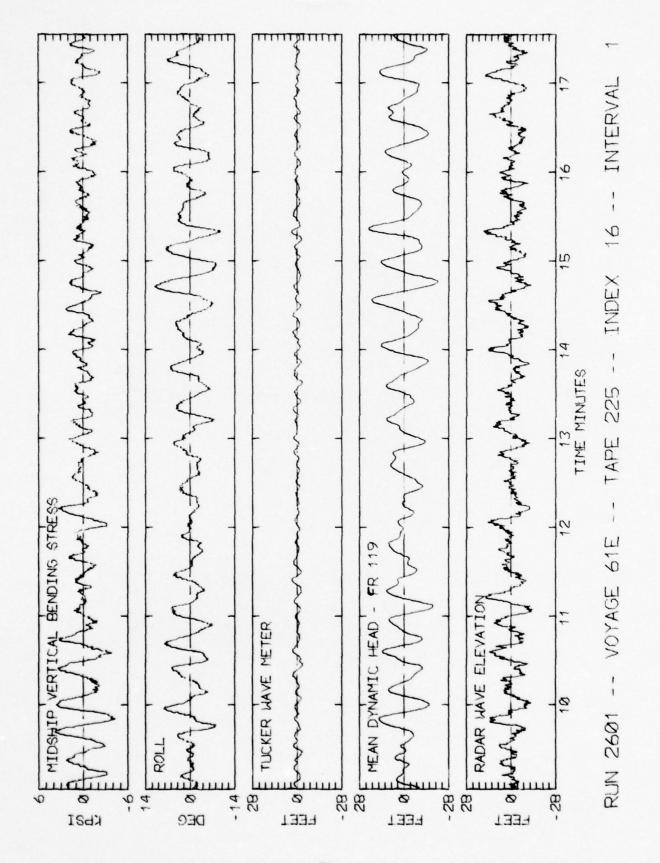


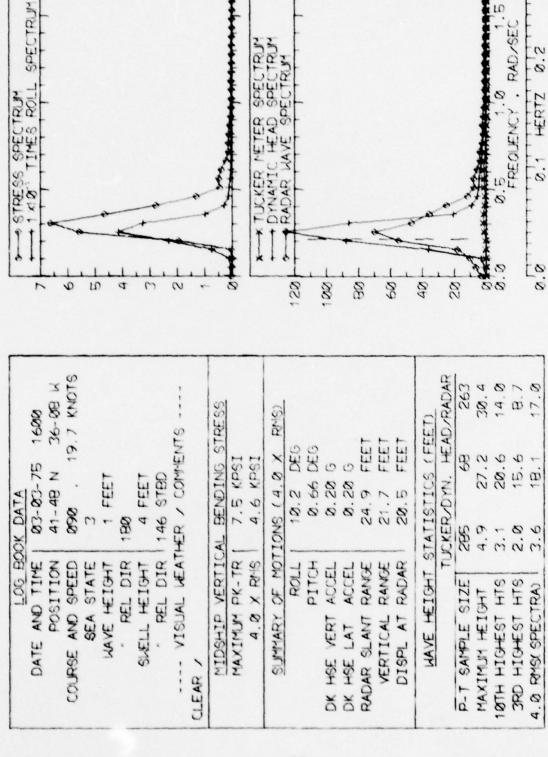
5.88

82

SPECTRUM

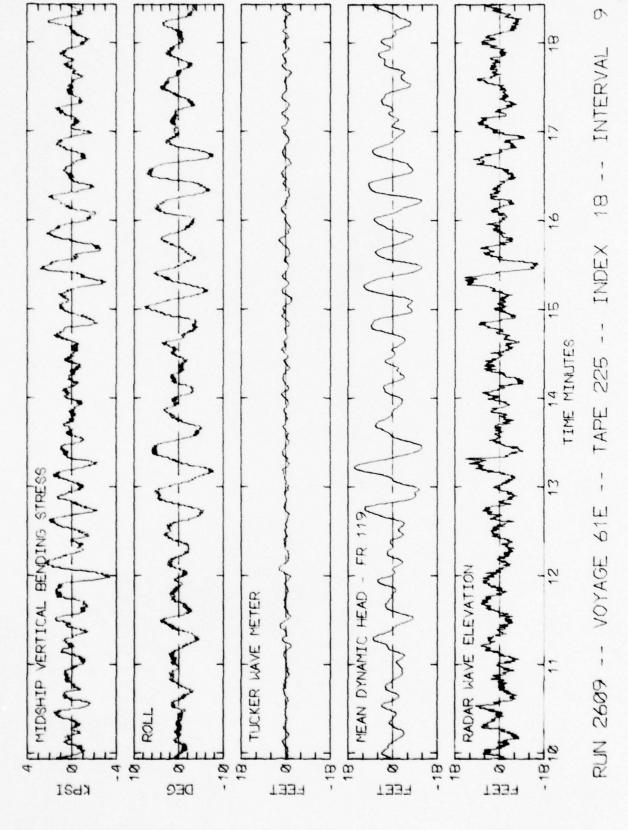
INTERVAL 16 ---- TAPE 225 -- INDEX RUN 2601 -- VOYAGE 61E





283

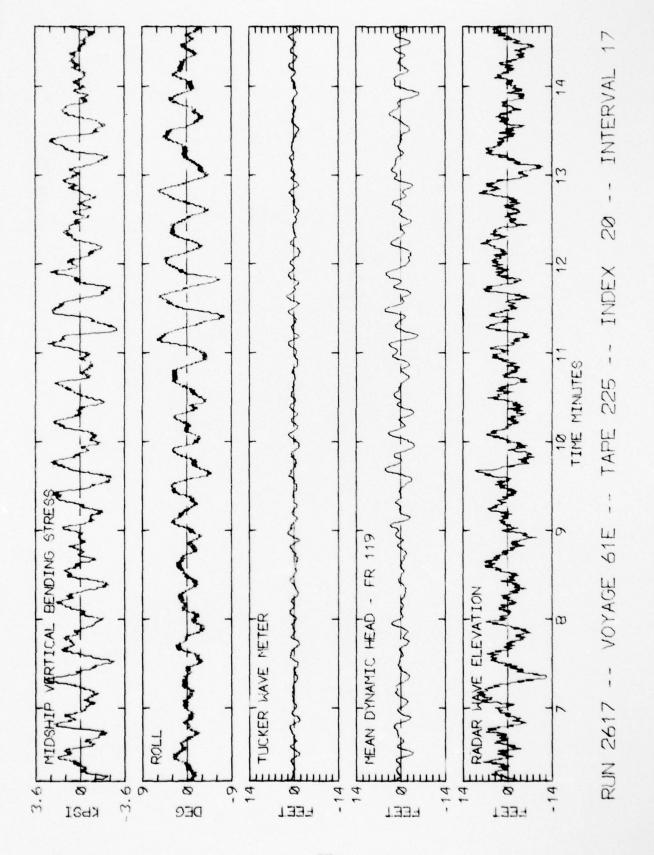
0 INTERVAL 18 INDEX 225 TAPE 61E VOYAGE RUN 2609 --

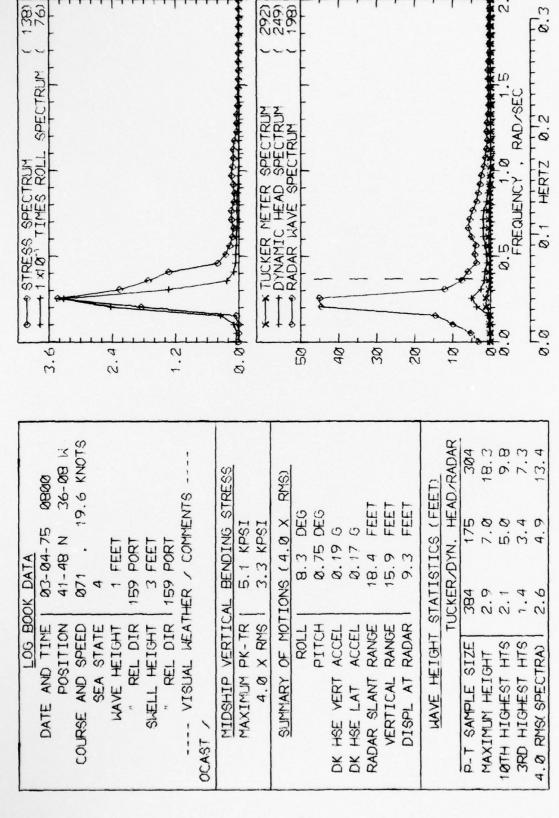


2 X 8 X 1 X 1 X 1 X 1 X 1 X 1 X 1 X 1 X 1		-	19	4		100	li.	1.1		8448	* TIKKER M		50 THADAN MA	-	180		1 2 1	800	3	20-	7	The state of the s	O *********	8.8	T.	
	19.8 KNOTS						MENTS		BENDING STRESS	15.	15.	X RMS)	DEG	DEG	9	9	FEET	FEET	FEET	(FEET)	HEAD/RADAR	142 328	9.7 22.9	.2 11.6	5.1 7.6	
<u> </u>	N 41-48 N		T 1 FEET	R 159 PORT	T 4 FEET	R 159 PORT	WEATHER / COMMENTS			R B.2 KPSI	S 4.5 KPSI	OF MOTIONS (4.8 X	L 8.2	H 8.75				E) 16.2	11.4	STATISTICE	TUCKER/DYN.	333 1	3.7	2.7	1.8	
DATE AND TIME	COURSE AND SPEED		WAVE HEIGHT	* REL DIR	SKELL RIGHT	REL DIR	VISUAL VE	CLEAR /	MIDSHIP VERTICAL	MAXIMUM PK-TR	4.0 X RMS	SUMMARY OF M	ROLL	PITCH	DK HSE VERT ACCEL	DK HSE LAT ACCEL	RADAR SLANT RANGE	VERTICAL RANGE	DISPL AT RADAR	MAVE HEIGHT STATISTICS (FEET)		P-T SAMPLE SIZE	MAXIMUM HEIGHT	10TH HIGHEST HTS	3RD HIGHEST HTS	

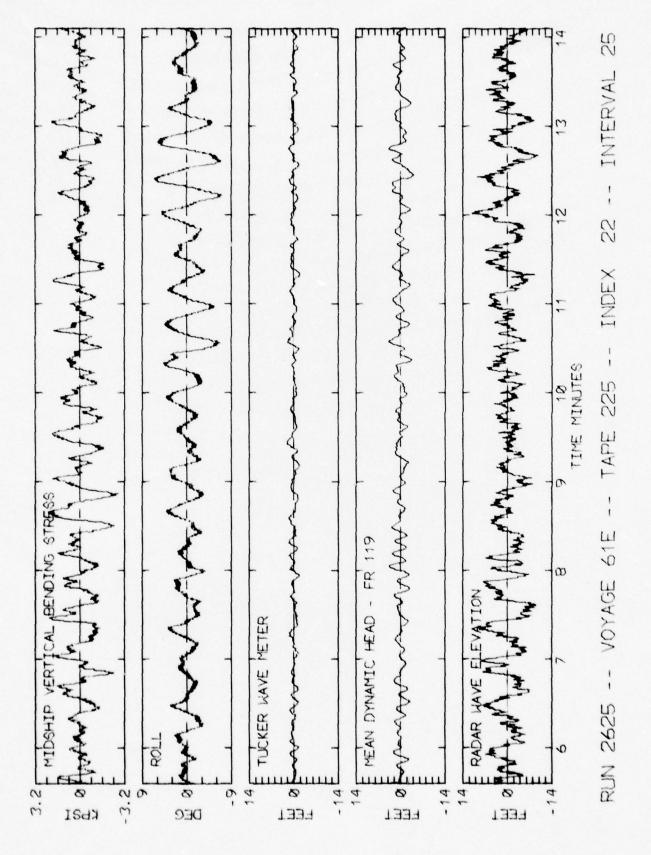
38 282 285 285 285 285 THIRTH RADISEC SPECTRUM METER SPECTRUM HEAD SPECTRUM JAVE SPECTRUM 8.2 HERTZ SPECTRUM INES ROLL

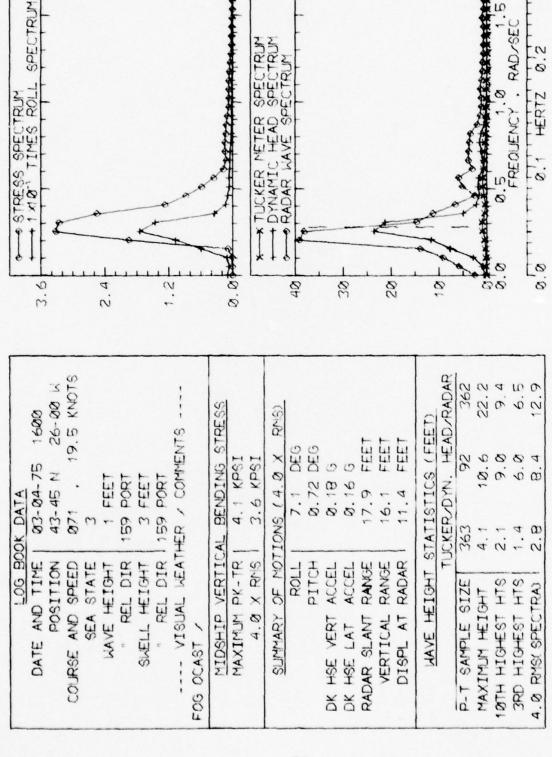
RUN 2617 -- VOYAGE 61E -- TAPE 225 -- INDEX 20 -- INTERVAL 17





25 INTERVAL 22 --INDEX 225 ---- TAPE RUN 2625 -- VOYAGE 61E



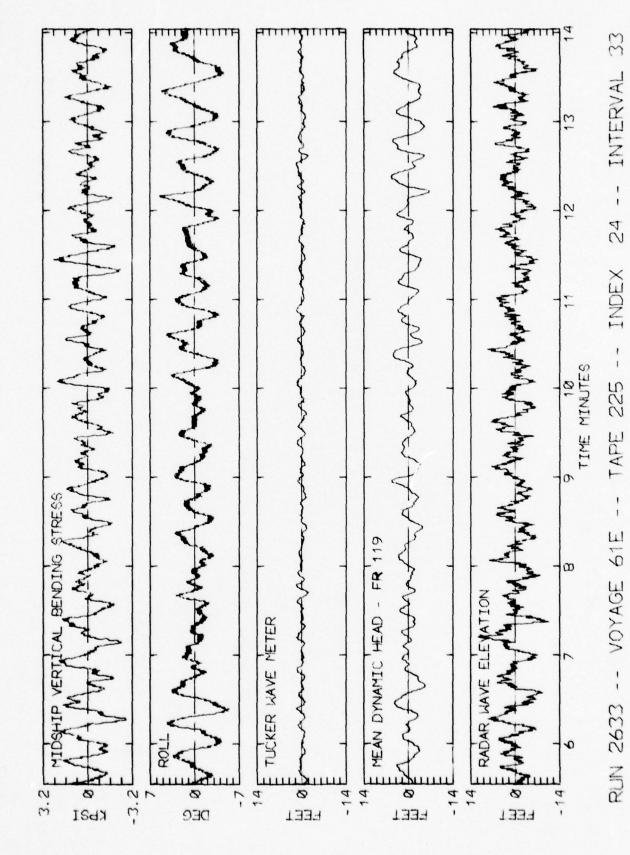


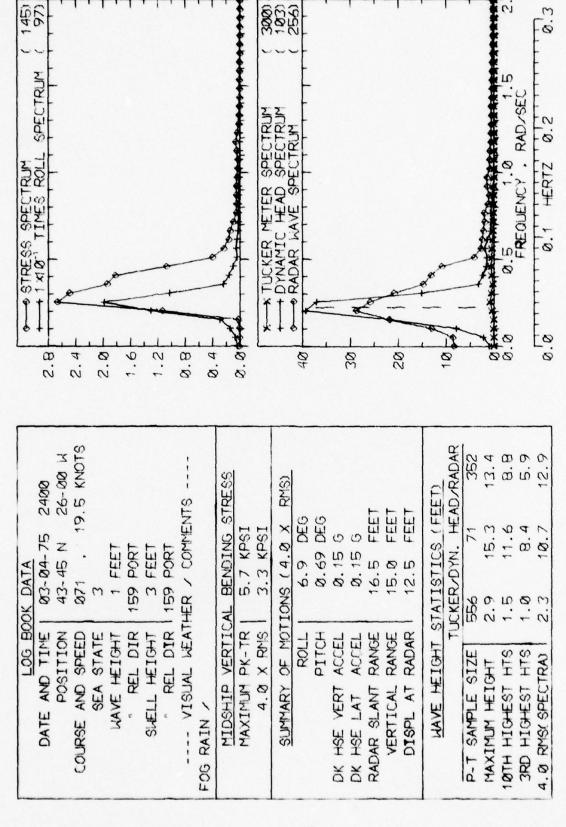
319)

146

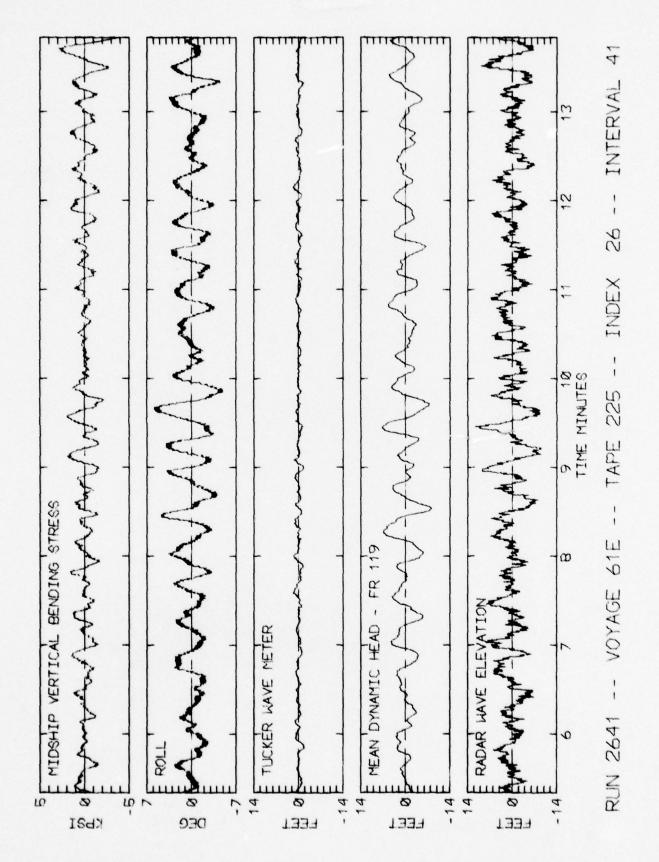
33 INTERVAL 24 --INDEX 225 TAPE 4 6 VOYAGE RUN 2633 --

0



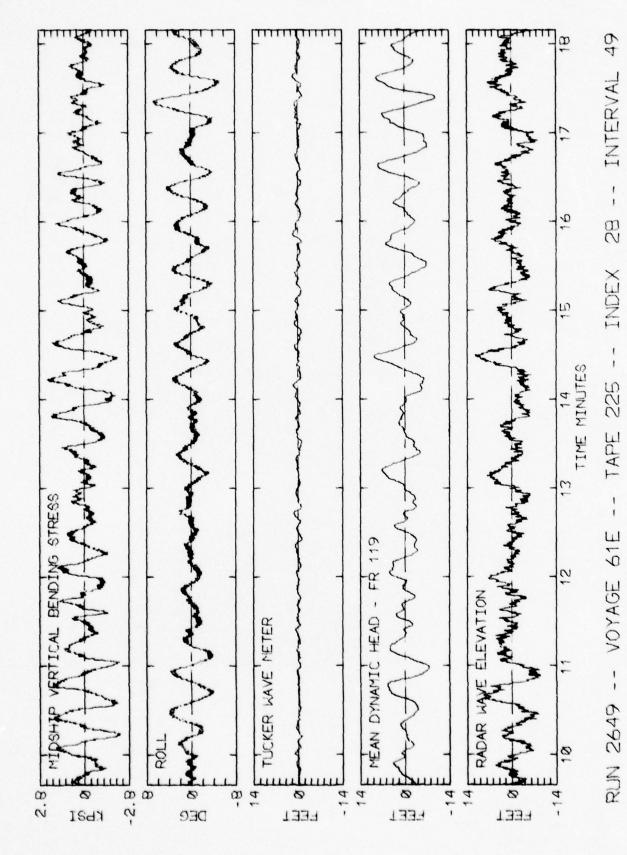


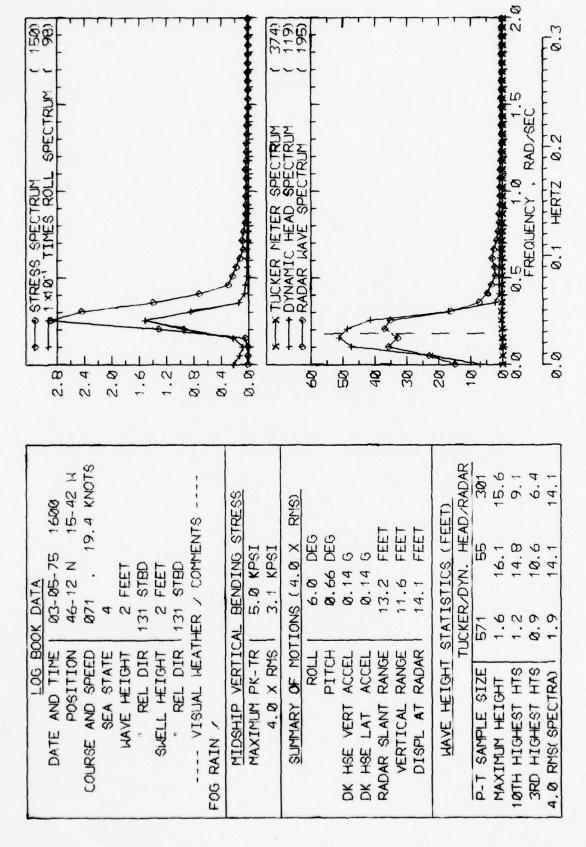
7 26 -- INTERVAL -- TAPE 225 -- INDEX VOYAGE 61E 1 RUN 2641



3 STRESS SPECTRUM (102)	BO RADAR WAVE SPECTRUM (293) 80 40	BONE OF FREQUENCY RADISEC
LOG BOOK DATA DATE AND TIME 83-86-75 8888 POSITION 43-45 N 26-88 W COURSE AND SPEED 871 , 19.5 KNOTS SEA STATE 2 WAVE HEIGHT 1 FEET SWELL HEIGHT 2 FEET REL DIR 159 PORT REL DIR	MAXIMUM PK-TR 4.8 KPSI 4.0 X RMS 3.2 KPSI SUMMARY OF MOTIONS (4.0 X RNS) ROLL 6.8 DEG PITCH 0.68 DEG DK HSE VERT ACCEL 0.15 G DK HSE LAT ACCEL 0.14 G RADAR SLANT RANGE 11.9 FEET	MAVE HEIGHT STATISTICS (FEET) TUCKER/DYN. HEAD/RADAR P-T SAMPLE SIZE 557 64 303 MAXIMUM HEIGHT 2.0 17.0 18.9 10TH HIGHEST HTS 1.2 13.8 9.8 3RD HIGHEST HTS 0.8 10.0 6.1 4.0 RMS(SPECTRA) 1.9 13.4 13.6

28 -- INTERVAL 49 TAPE 225 -- INDEX RUN 2649 -- VOYAGE 61E --





57 INTERVAL 30 --INDEX 225 TAPE VOYAGE 61E RUN 2657 --

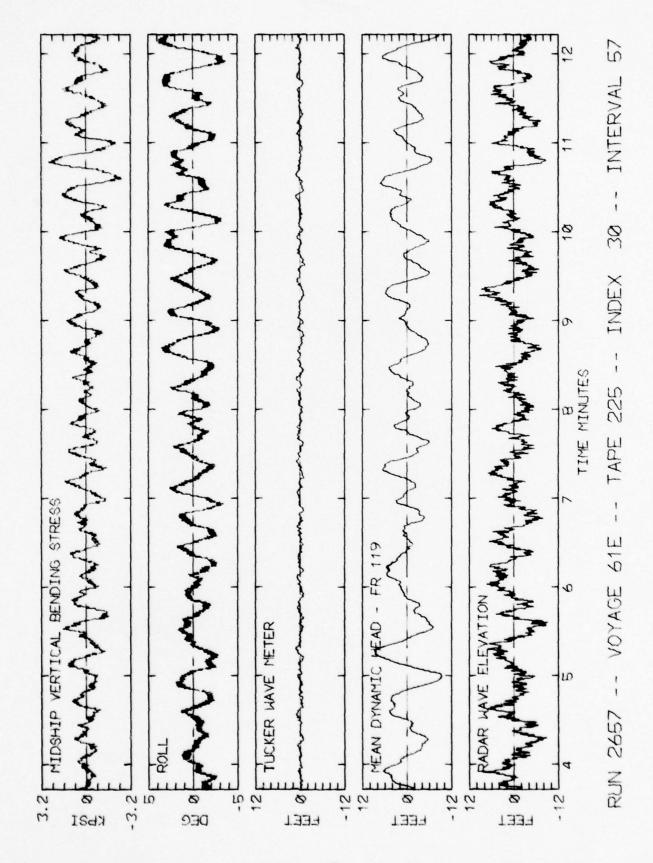


TABLE 11a

CW.

SUMMARY OF TMR LCG-BOOK DATA CORRESPONDING TO INTERVALS SELECTED FOR WAVE METER DATA REDUCTION (PAGE 1 OF 2)

SEA LAND MC LEAN : 1974-1975 WINTER SEASON : VOYAGE 61 WEST

SEA/AIR TEMP	52/52	3/5	2/6	2/2	8/6	8/5	8/6	58/60	3/6	5/5	1/5	9/8	5/0	64/52	64/52	66/45	68/68	-
ORAFT FT.																		
PROP	133.5	120.0	0	•	•	_	01	-	3	-	0	10	0	0	0	01	+	_
SPEED KT.	33.1	29.3	0	2	2	-	-	~	9	2	-	-	-	17.1	17.1		18.0	•
COURSE	244	544	942	273	273	273	273	273	273	273	270	270	270	270	270	270	27.0	27.0
LONGITUDE COURSE	30-47 W	7-36	-04	5-64	20-5	2-40	2-48	3-40	3-48	2-48	2-48	0-37	0-37	0-37	6-37	0-37	6-37	18-37
LATITUDE		. 1	8-53	8-53	9-16	67-6	52-5	67-6	67-5	67-5	67-6	9-54	75-6	75-6	75-6	9-54	75-6	6-54
TIME (GMT)	2400	70	0	70	2 8	20	60	03	6 9	2 5	8 8	3 4	0 5	99	86	23	48	69
DATE	03-11-75	-	13-	13-	14-	15-	15-	23-15-75	15-	16-	16-	16-	16-	03-16-75	16-	83-16-75	16-	83-17-75
INTV NOV	13	37	65	61	11	33	37	41	46	64	53	5	9	11	14	18	21	25
INDX NO.	31	13	13	16	19	52	56	27	28	53	30	32	32	33	34	35	36	37
TAPE NO.	229	553	558	528	231	231	231	231	231	231	231	233	233	233	233	233	233	233
P.L. RUN NG.	2713	2737	5149	2761	2811	2833	2837	2841	2846	5840	2853	2985	2986	2911	2914	2918	2921	2925

TABLE 11b

SUMMARY OF TMR LCG-BOOK DATA CORRESPONDING TO INTERVALS SELECTED FOR WAVE METER DATA REDUCTION (PAGE 2 OF 2)

SEA LAND MC LEAN : 1974-1975 WINTER SEASON : VOYAGE 61 WEST

15

0.1.		EL WIN	REL	MAVE	REL	4-SH	ELL->					
0	SEA	DIRISPEED	WAVE	H	SWELL	11	HT LENGTH					
NO N	A	-	DIR	FT.	018	F T.	FT.	VISUAL	WEATHER	/ TER	L06-800K	COMMEN
2713	9	1779/13	1779	2	1165	~	500	PT CLOY	1			
2725	4	-	715	-	1165	~	609	CLEAR				
2737	4	-	35	-	196	~	600	DCAST				
5749	•	-	550	-	21P	7	463	_	/ /			
2761	7	875/ 5	875	-	878	2	692	PT CLDY	, ,			
2811	-		425	-	875	~	600	_				
2833	2	2	138P	2	48P	~	605	U				
2837	9	~	117P	7	48P	4	400	d				
2841	1	3	48P	ę	48P	9	700	U				
2846	7	3	486		48P		609	CAS				
5849	7	3	3 P	28	36	20	683	CA				
2853	6	25/4	225		0		688	D				
5965	7	5/3	675		675		623	CAS				
2986	7	5/3	675		675		660	U				
2911	9	75/2	675	18	675	16	600	_	'			
2914	9	75/2	675		675	18	629	_	1			
2918	2	75/2	675		675	18	699	_	/ ENO	MANUAL	. RECORD	
1262	4	675/15	675	ę	675	9	683	PT CLDY				
2925		75/1	675	~	675	~	862	1	. / /			

TABLE 11c

COMPARISON OF TMR RESULTS FOR MIDSHIP VERTICAL BENDING STRESS WITH CORRESPONDING RAW DIGITIZATION RESULTS AT DAVIDSON LABORATORY

SEA LAND MC LEAN : 1974-1975 WINTER SEASON : VOYAGE 61 WEST

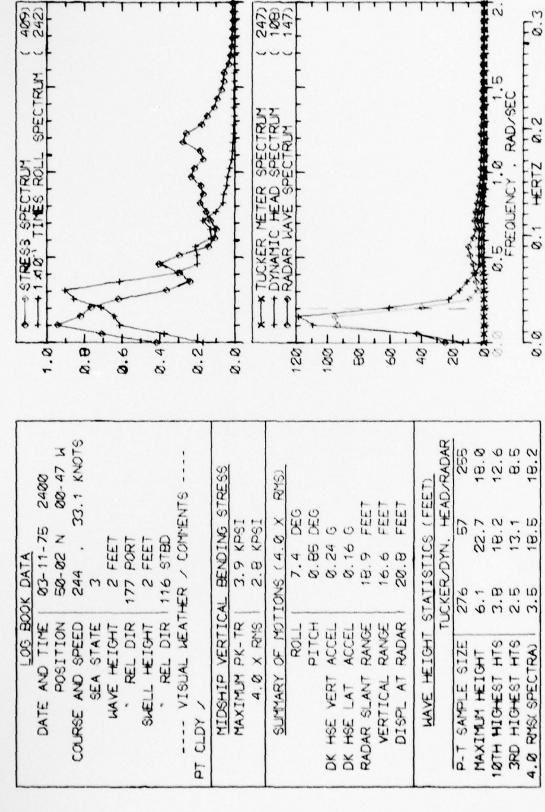
35>		(9)	•	(3)			1.17	1.06	1.19	1.48	11.0	1.11	1.01	1.28	1.00	1.86	1.11	8.93	10.1	1.22	1.07	1.09	1.05	1.15	1.04
* <column ratios=""></column>		(9)	,	3+51			1.17	1.36	1.20	05-		.11	. 21	1.20	. 84	.86	.86	. 78	64.	96.	.85	.93	.86		1.24
JU UM		_		(3			1 91	13																	88
33		(7)	•	(4)			1.1	1.1	1.0	-	8.0	1.6	1.6	1.05	1.6	0.0	0.0	0.8	0.0	0.0	0	0	0.8	1.	1.6
*		4	\$	•	4	*	*	4	4	4	4	*	*	4	4	4	٥	4	٥	4	4	•	٥	*	•
ATION	REL	MEAN	STRESS	KPSI	(8)		0.08	1.46	-8.47	8.22	1.90	9.65	2.27	0.06	0.18	0.35	3.65	2.71	0.22	2.22	0.12	-0.73	2.13	0.19	0.13
91GIT [2A]	2.83X	(SAMPLE	(SWa	KPSI	(7)		1.98	16.1	1.79	1.53	2.84	1.30	1.11	1.84	5.49	3.94	4.51	5.25	7.39	5.93	4.15	3.45	5.99	1.95	1.20
-1.0	ANGE	RECORDED	EXTREMES	KPSI	(6)		4.56	4.24	4.56	3.54	4.44	3.01	2.62	2.46	6.36	10.01	12.93	14.20	17.56	17.03	10.93	9.52	6.77	4.65	3.83
0	•	4	•	4	4	0	4	*	4	4	•	•	•	•	43	*	*	4	*	43	٠	4	o	*	43
;		00	STRESS	SI	(5)		8.89				2.00	32.6	2.20	03.3	1.20	2.18	3.34	2.78	4.74	3.85	2.72	1.56	1.43	19.3	20.0
	52	-	STRESS	S	(4)		1.78	1.78	1.69	1.39	2.44	1.22	1.86	56.2	2.43	4.18	4.92	5.94	7.58	6.48	4.45	3.59	3.16	1.86	1.11
RESULTS-		•	STRESS		(3)		3.91	4.21	3.84	2.53	5.15	2.72	2.59	2.85	6.38	9.41	11.64	15.33	17.38	13.96	12.19	8.71			2.93
TMR	. DN	ST	MODE	a	2		0	63	~	9	8	0	0	2	14	37	43	69	72	85	37	2.5	11	3	0
>		I	INDUCE	U			6	80	15	16	12	14	17	165	18	16	16	14	14	15	15	15	15	14	123
	0	4	*		4	*		4	*		•				44				44		*			4	4
		0.1.	NO.	N.C.			71	72	2737	14	16	2811	83	2837	84	84	84	85	36	2986	91	91	91	35	2925

TABLE 11d

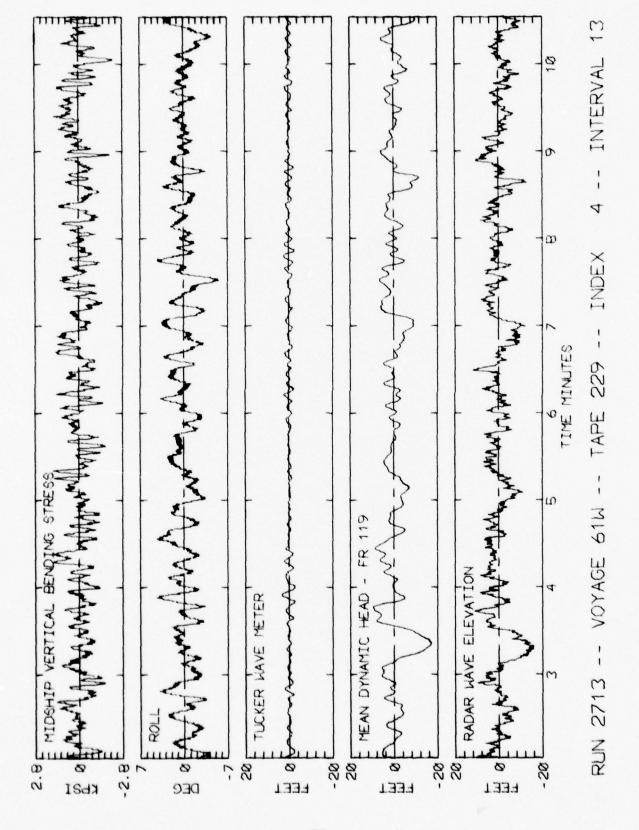
SUMMARY OF RAW DIGITIZATION RESULTS FOR RADAR RANGE ROLL, PITCH, DECK HOUSE ACCELERATIONS, AND TUCKER METER

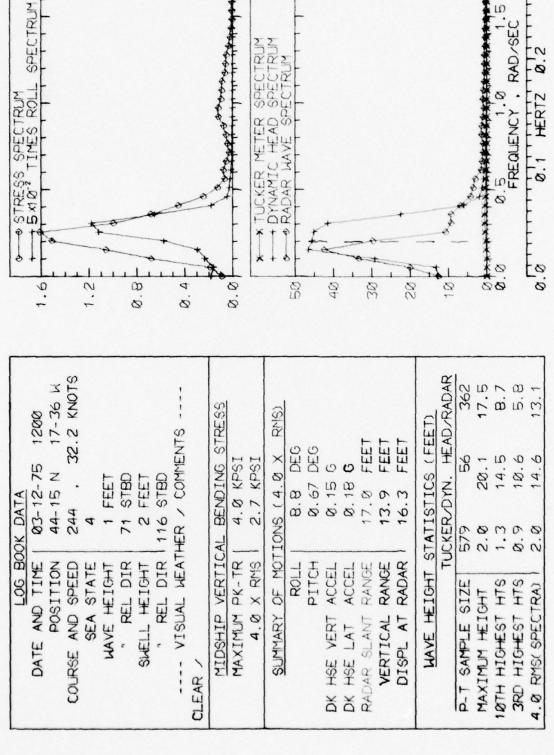
SEA LAND MC LEAN : 1974-1975 WINTER SEASON : VOYAGE 61 WEST

RADAR>< ROL RECORDED 4.0 R	050 4.8 R	050 4.8 R	B R		00	RDED	•	RECO	ROE	4.0	RECO	ROE	4.8	REC	DRUED	4.2	RECO	80
2	2	2		(RMS)	×	EME	(RNS)	×	N	Y	×	E	2	X	EME	(SHS)	×	w
u	u	u		DEG	DEG	LL.	w	DEG	w	(3)	(5)	(5)	(3)	3	(3)		-	u.
. 16.		-16		7.6	5.	80 1	8.8	2.2	-1.3	3.24	0.2	-0.5	3.16	0.1	-2.1	3.	3.	-3
. 14.		-13		8.8	5.	. 8	1.0	2.2	6.3-	0.15	0.1	-8.1	0.18	0.1		2.	,	- 2
16. 1713		-13		4.4	3.	-4.	1.6	6.5	-1.3	0.24	0.5	-0.2	0.18	8.1		2.	7	-2.
. 12.		-13			3.	-3.	6.9	6.3		0.21	9.5	-0.5	9.11	6.1		2.	?	- 2.
. 17.		-16			2.	.5.	1.2	5.2	-1.4	3.24	9.5	-0.5	0.10	0.1	-8.1	3.	2.	-3.
. 12.		-18			3.	- 4-	2.7	2.2	6.3-	0.17	8.1	-0.1	9.16	0.1		2.	2.	-2.
. 6		-8			1.	-4.	6.7	2.2	6.8-	9.16	0.1	•	62.0	9.1	-0.1	2.	۲.	-1-
		-11		2.7	. 4	-1:	2.7	2.1	-1.8	3.17	0.1	-0.1	9.29	2.1		1:	-	-
. 16.		-29			5.	-2.	1.3	2.7	-1.6	9.39	6.3	•	0.11	•	-8.1	3.	2.	-3
. 28.		-37			7.	-5.	1.6		-1.6	85.0	9.4	•	0.12	0		3.	3.	-3.
. 27.		-39		3.7	3.	-3	1.6	1.8	-1.7	8.43	7.0	7.0-	0.11	0.1	-0.1	4.	3.	-4-
. 33.		-50			2.	. 7-	1.9	1 .4	-1.8	0.50	9.4	4.0-	0.12	0		5.	3.	-4-
. 41.		-61			-1	-7.	5.4		-2.8	3.62	9.5		•	6.1	-2.1	ď	. 4	-4.
. 48.		-54			1.	-7.	•	1.3	-1.8		9.5	-0.5	•	0		4.	4.	-4-
. 31.		74-		4.8	2.	-7.		1.2	-1.8		9.6	-0.4	-:	0.1		5	4.	-4-
. 30.		-41			3.	-1.		5.3	-1.7	9.46	3.4	7.0-	-:	9.1			4.	-4-
. 26.		-31			3.	.6-	1.4	8.2	-1.6	0 7.0	6.3	-0.4	9.15	9.1	-0.1	5.	3.	-4-
. 14.		-23		4.3	3	-5-	1.0	8.5	-1.2	3.25	3.5	-0.5	3.12	9.1		3.	3.	-3.
. 6		13		5.6	-	-3.	2.7	2.2	-1.2	0.15	0.1	-0.1	63.0	9.1	-0.1	5.	۲.	-2



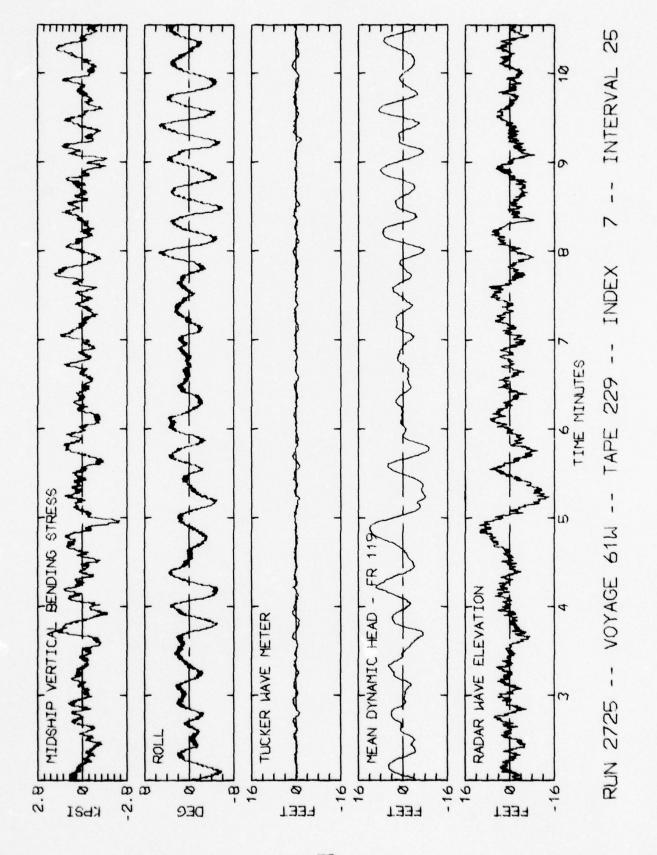
5 INTERVAL 4 --INDEX 229 --VOYAGE 61W -- TAPE RUN 2713 --

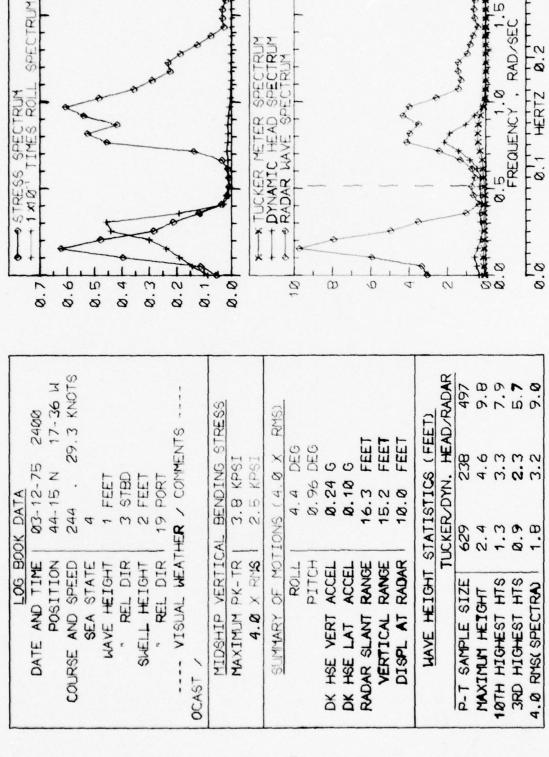




193

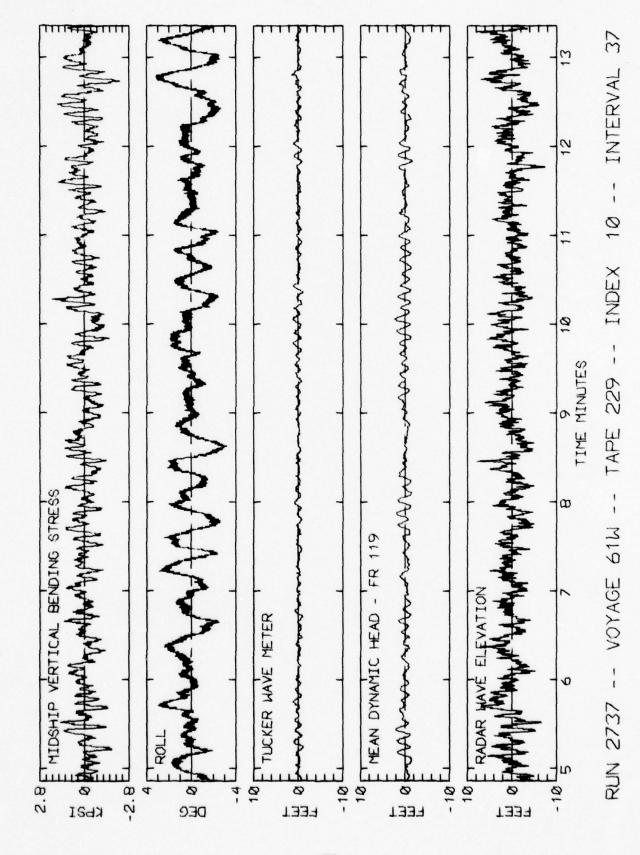
35 INTERVAL 1 ~ INDEX 229 --TAPE 1 61V VOYAGE

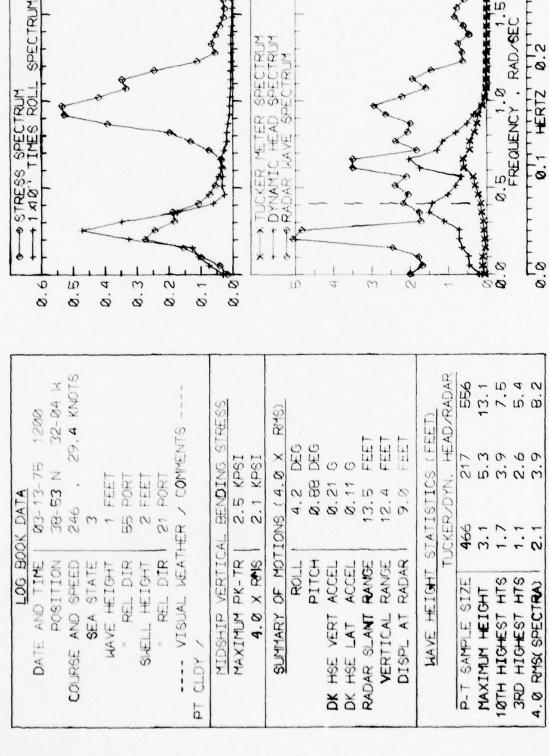




166

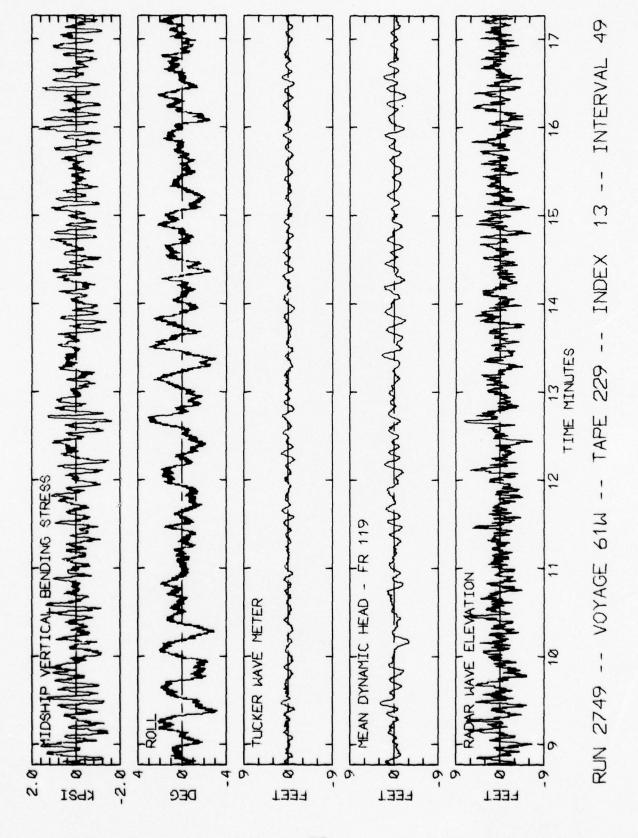
37 INTERVAL 10 ---- INDEX 229 TAPE WOYAGE 61W

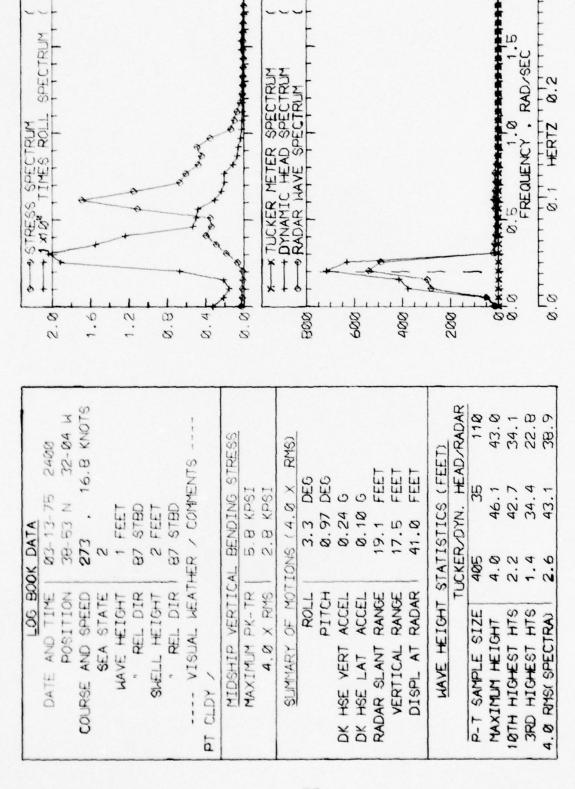




181

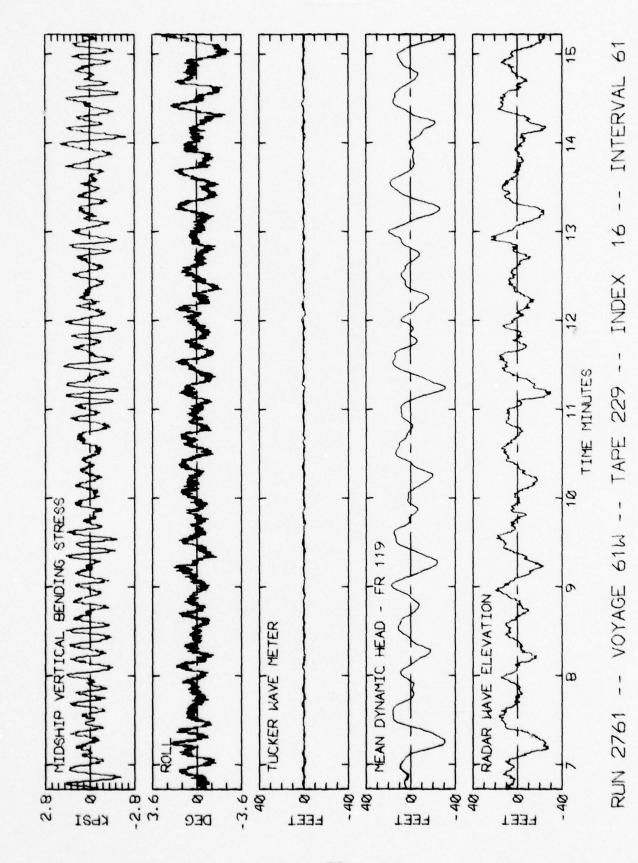
40 INTERVAL 13 --INDEX 229 --TAPE VOYAGE 61W RUN 2749 --

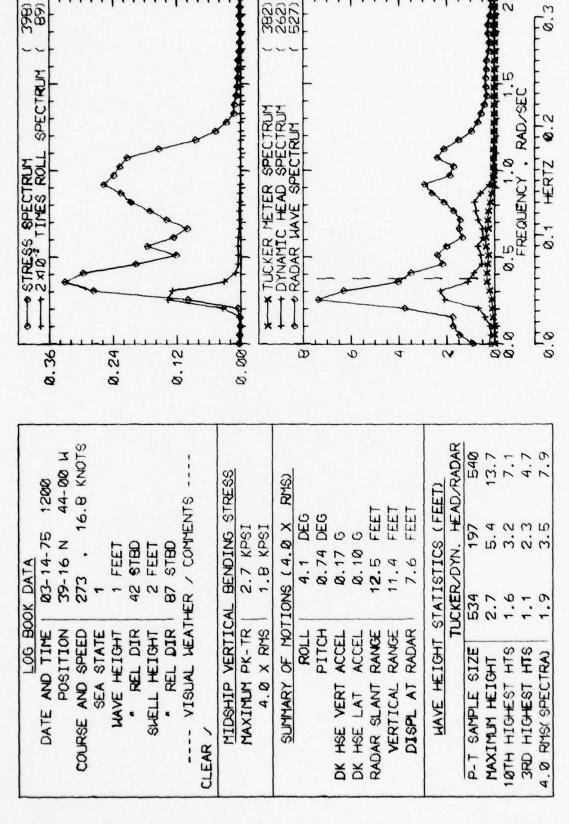




264) **84**) 97)

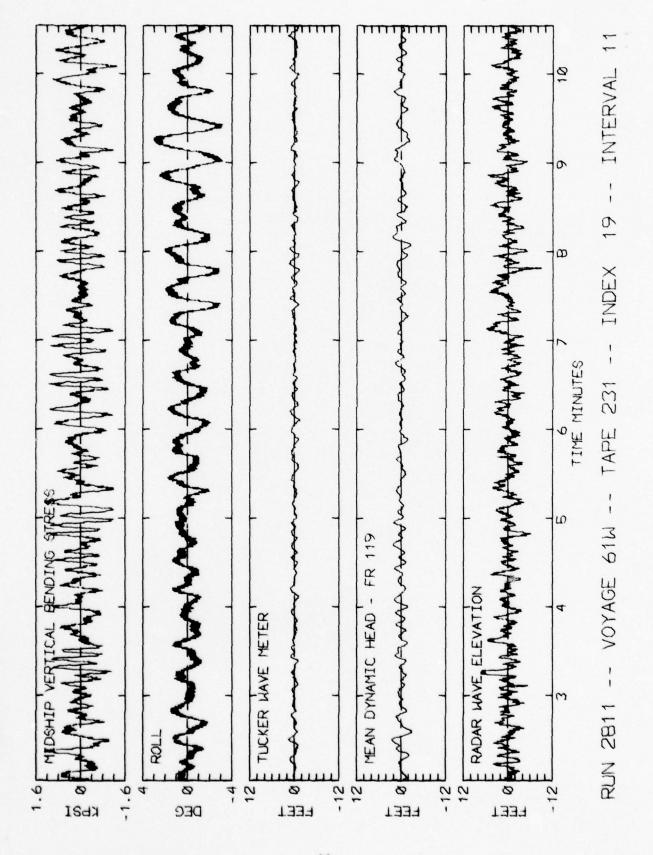
6 INTERVAL 16 --INDEX 229 --TAPE 675 VOYAGE RUN 2761 --

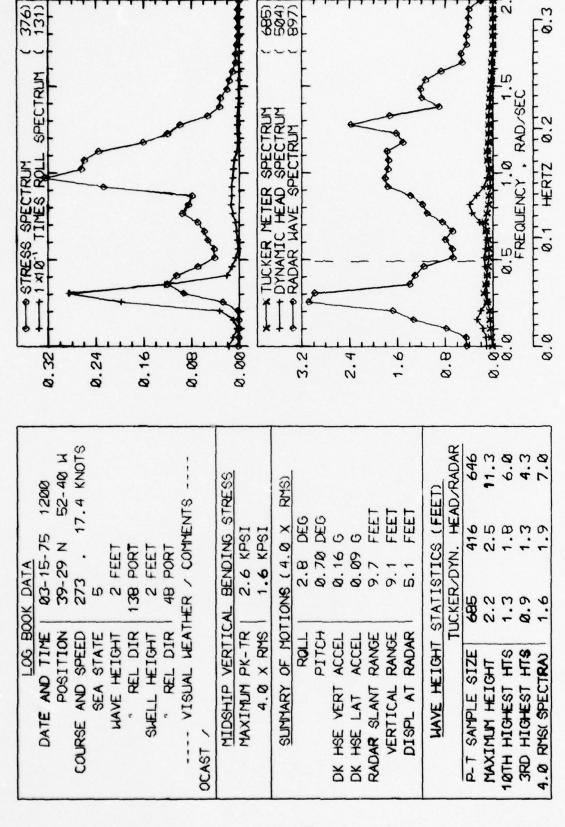




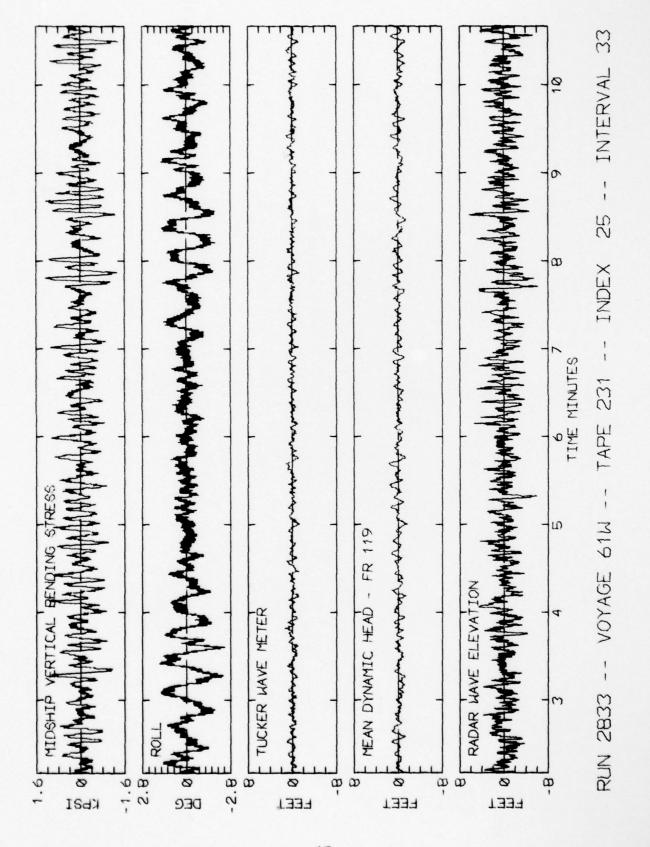
INTERVAL 19 --INDEX 1 231 TAPE 61N VOYAGE RUN 2811

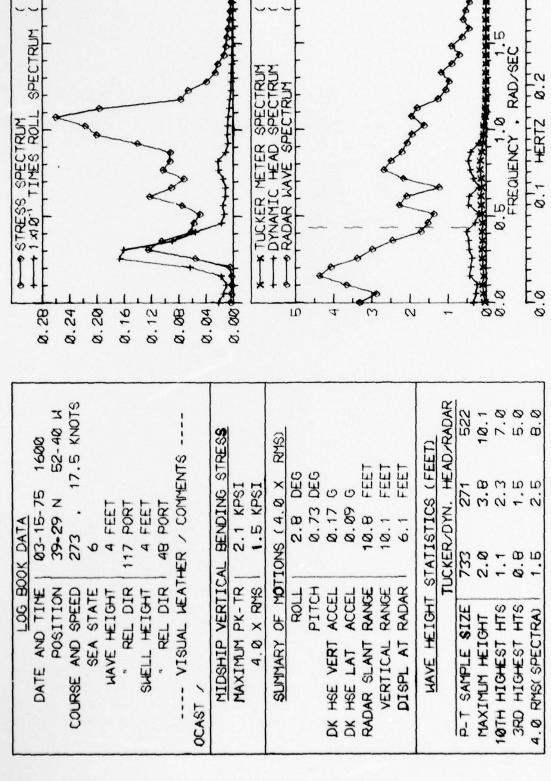
Fo





INTERVAL 25 --INDEX 1 231 TAPE VOYAGE 61W RUN 2833 --

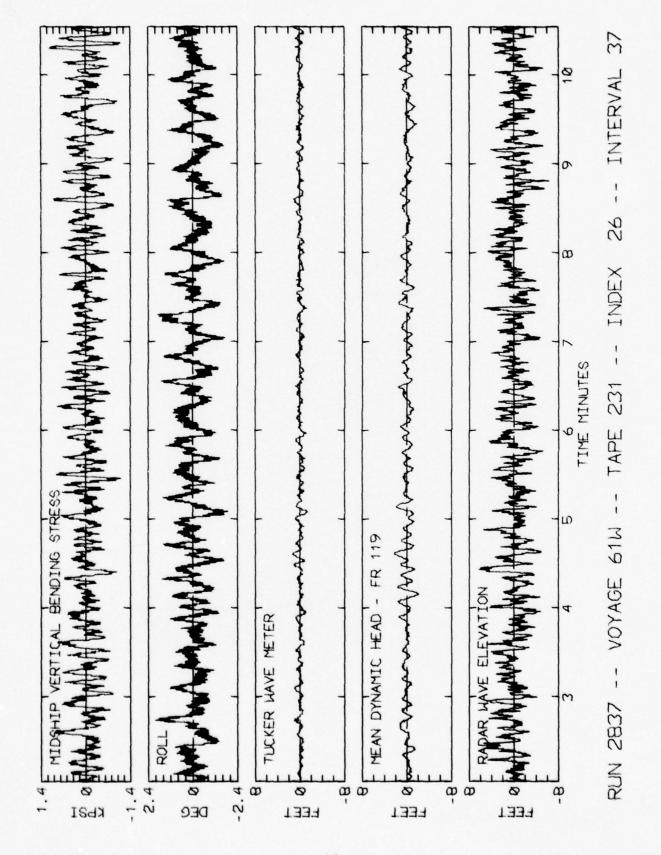


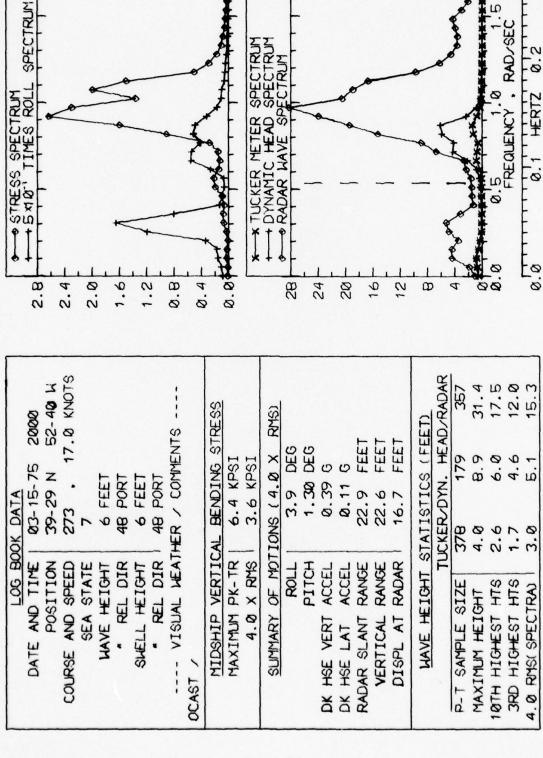


515) 407) 752)

422

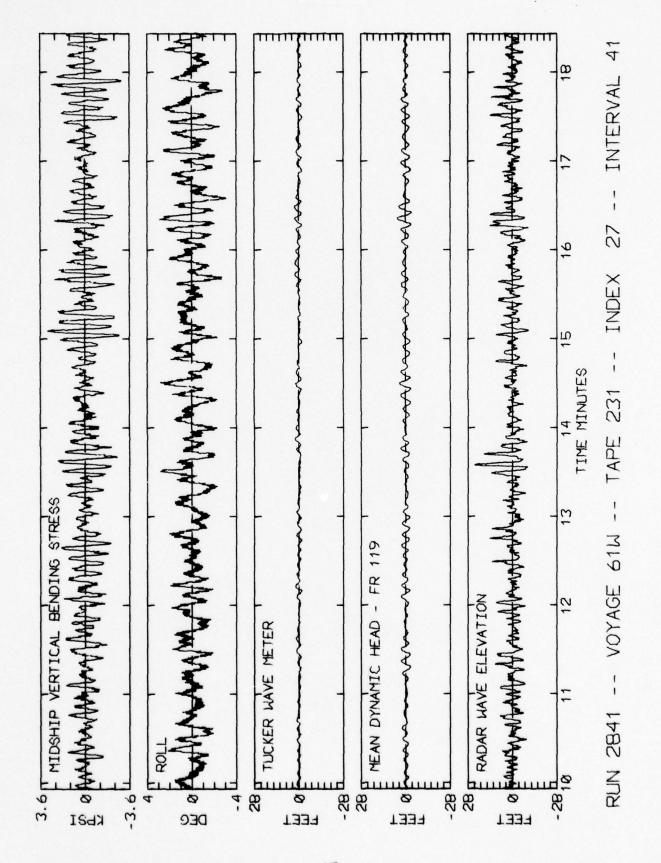
37 INTERVAL 1 26 INDEX 1 231 TAPE **61**2 VOYAGE

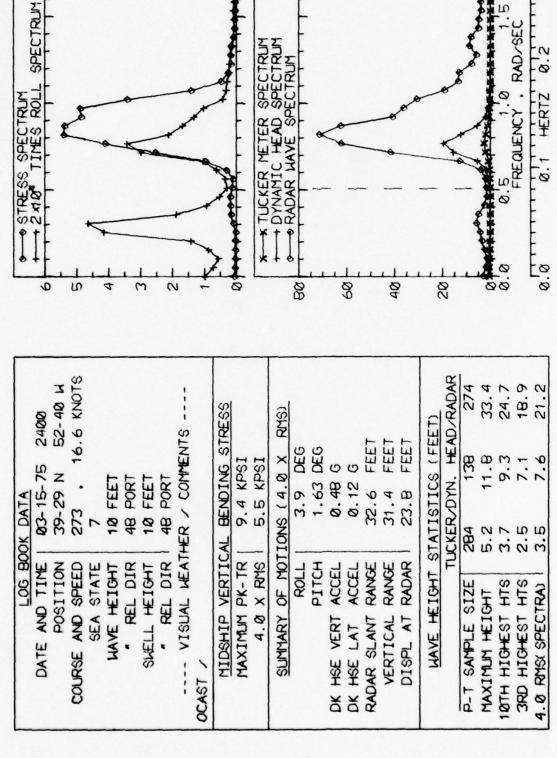




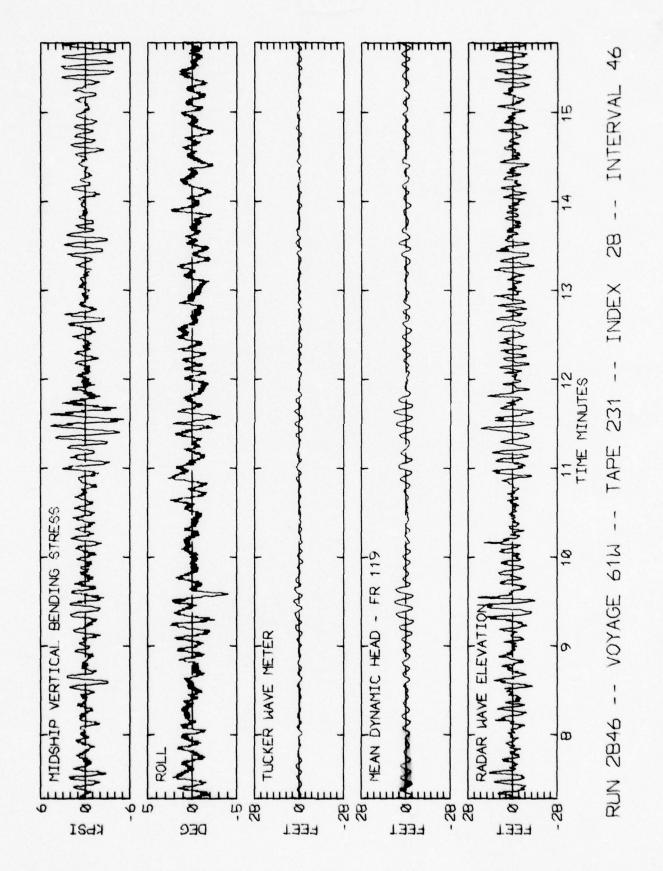
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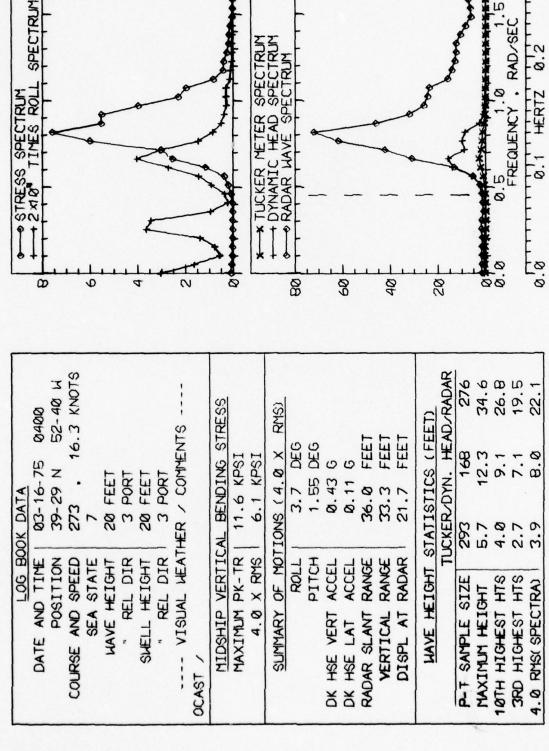
4 INTERVAL 1 27 INDEX 1 231 TAPE 1 61Z VOYAGE 1 RUN 2841



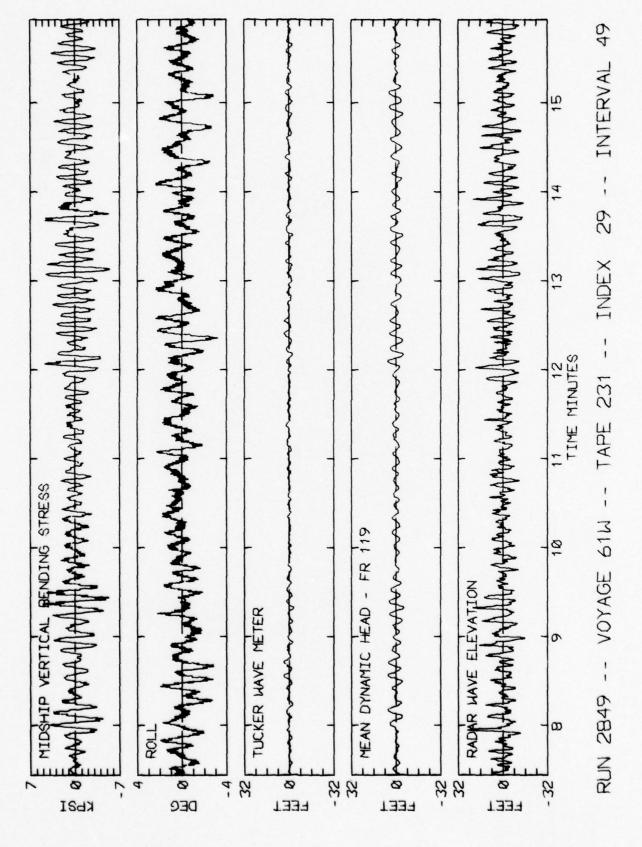


46 INTERVAL -58 -- INDEX 231 TAPE ! VOYAGE 61W RUN 2846 --



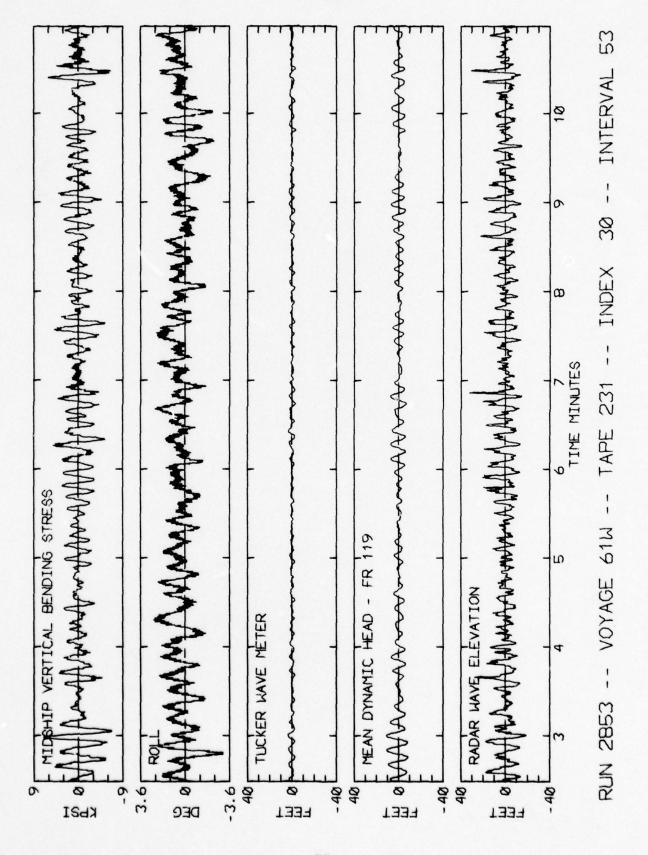


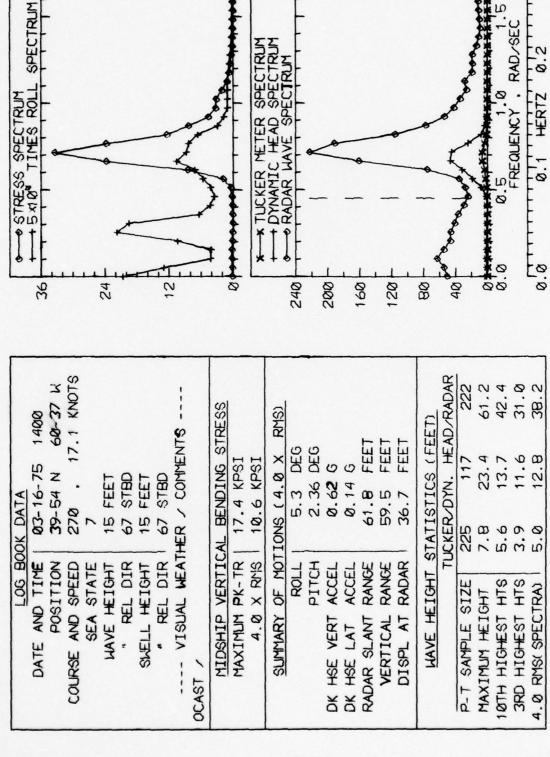
49 INTERVAL 29 --INDEX 1 231 TAPE ! 61 전 VOYAGE RUN 2849 --



14 CTRESS SPECTRUM (178) 12 CTRUM (296)	D 9 7 C	* TUCKER NETER SPECTRUM (187)	A RADAR MAVE SPECTRUM	20 -
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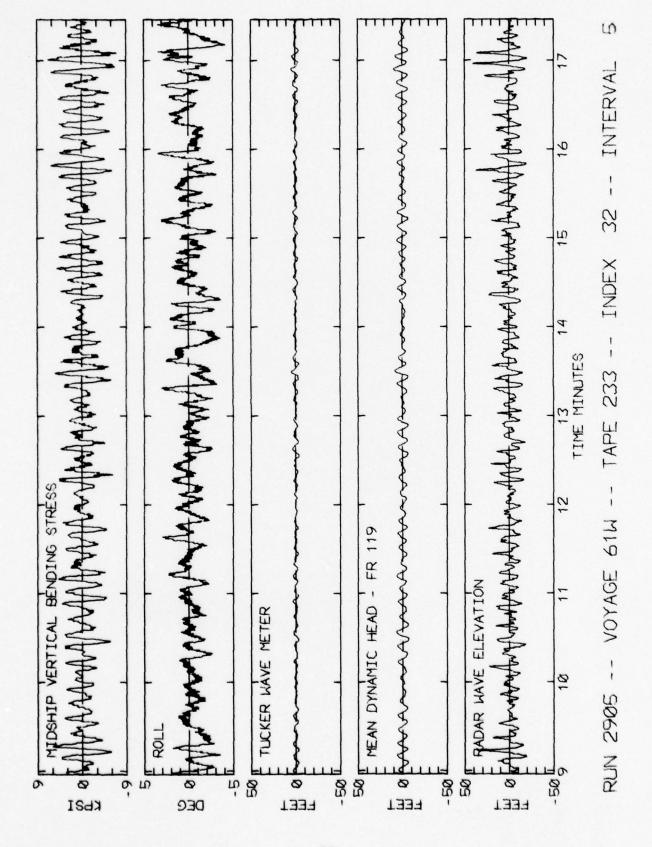
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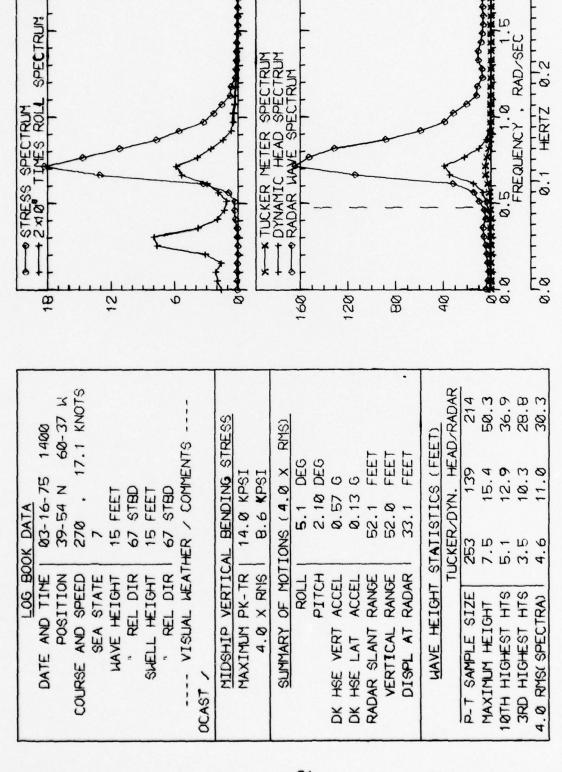




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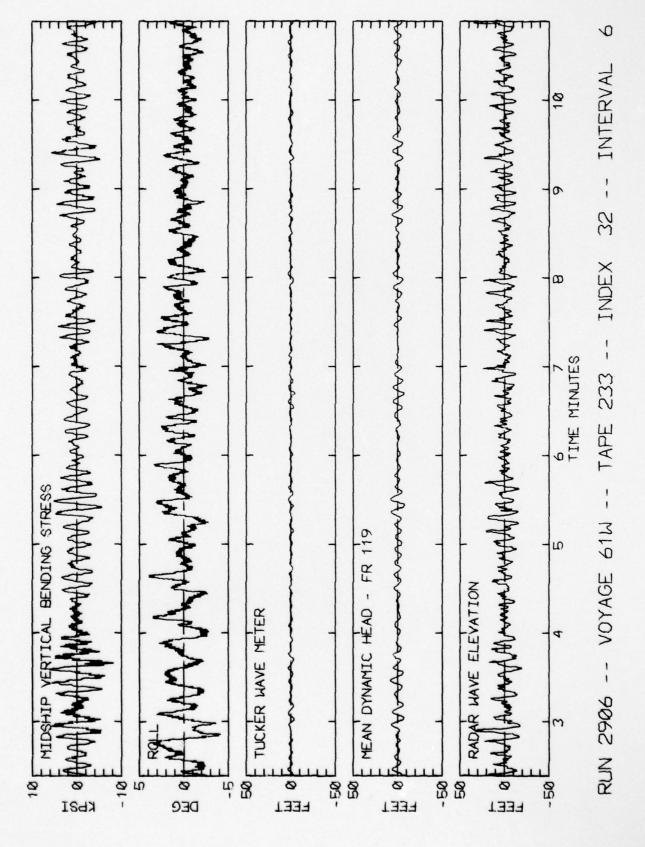
5 INTERVAL 32 --VOYAGE 61W -- TAPE 233 -- INDEX RUN 2905 --





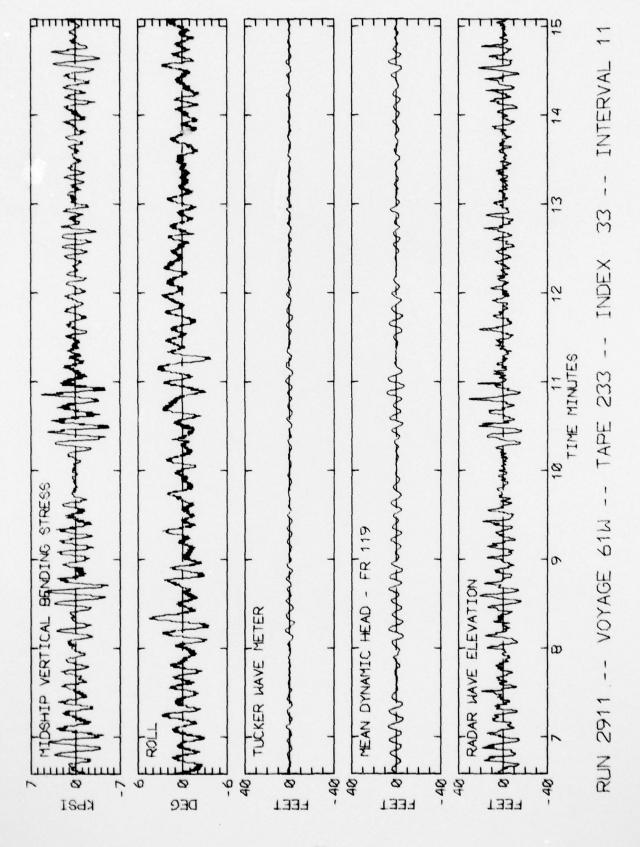
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0 INTERVAL 32 --233 -- INDEX -- TAPE RUN 2906 -- VOYAGE 61W



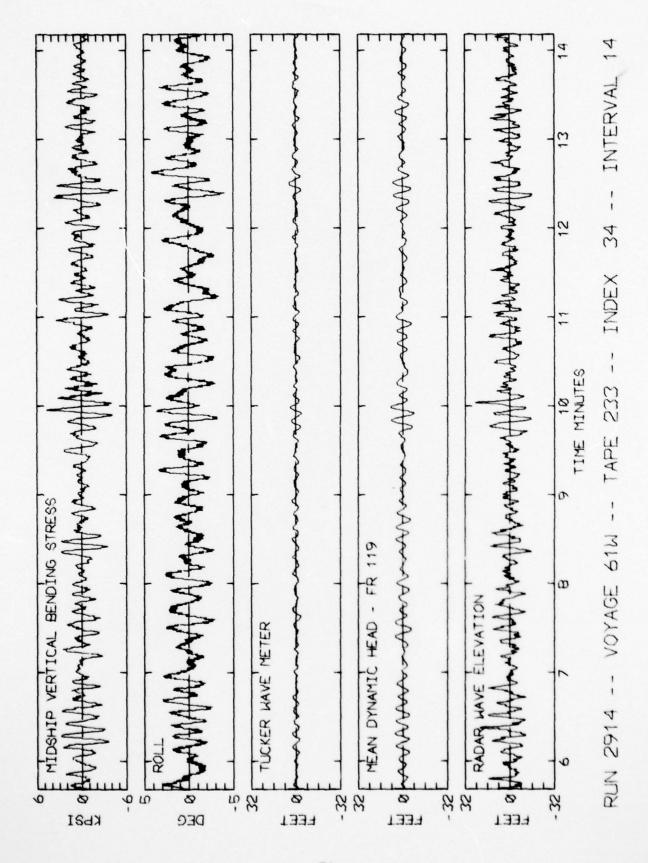
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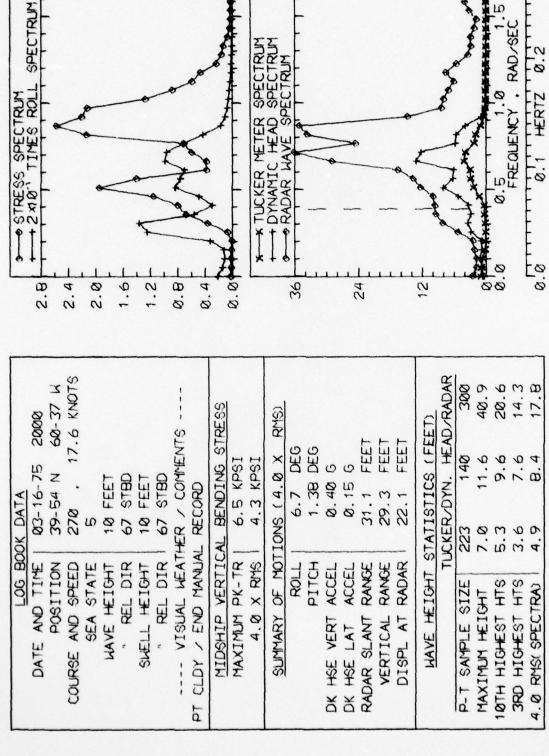
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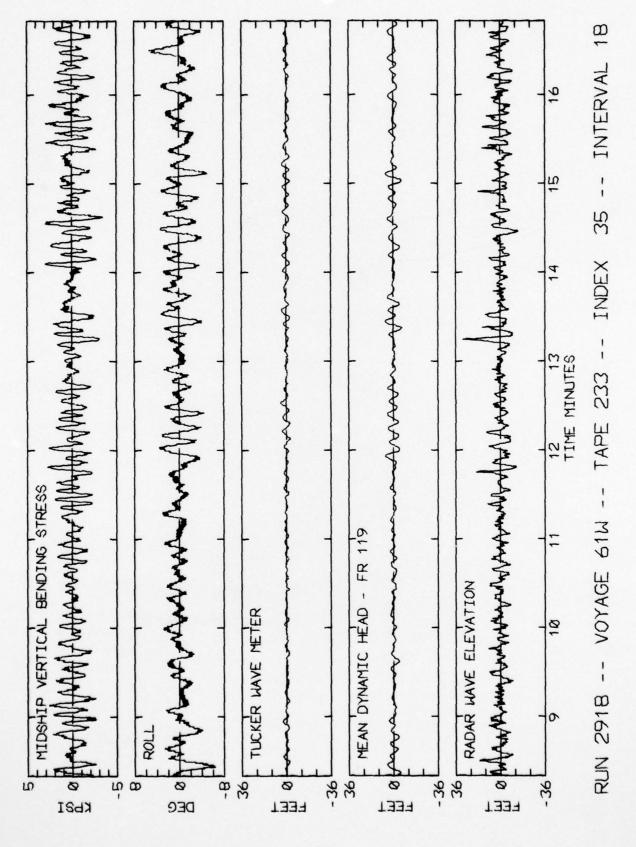
RUN 2914 -- VOYAGE 61W -- TAPE 233 -- INDEX 34 -- INTERVAL 14

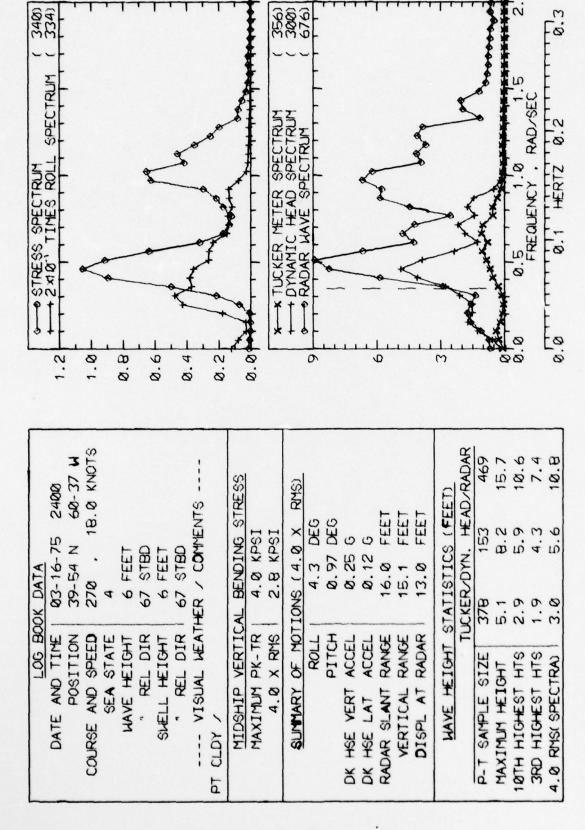




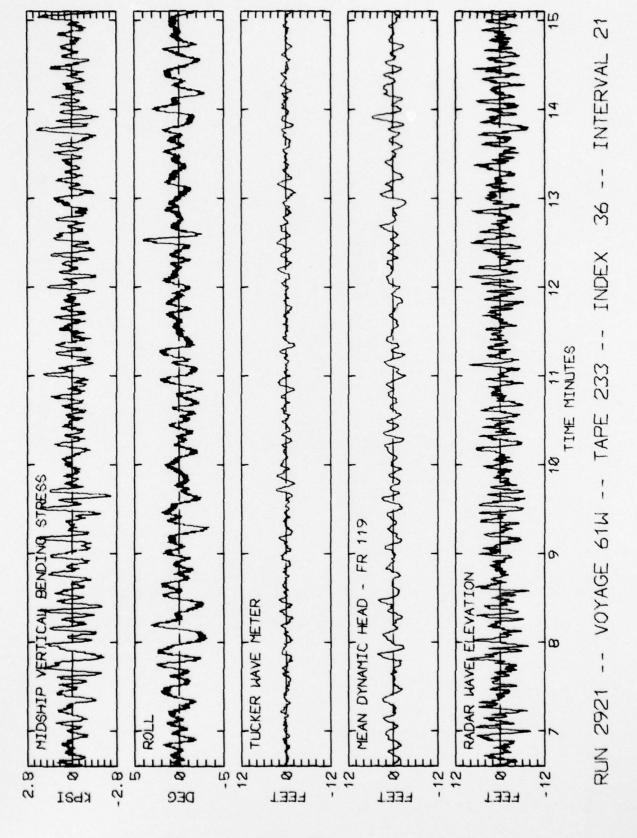
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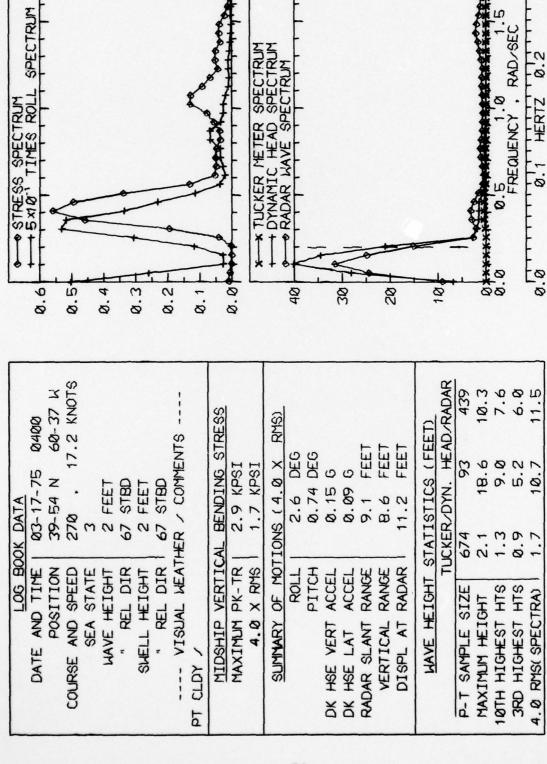
6.3





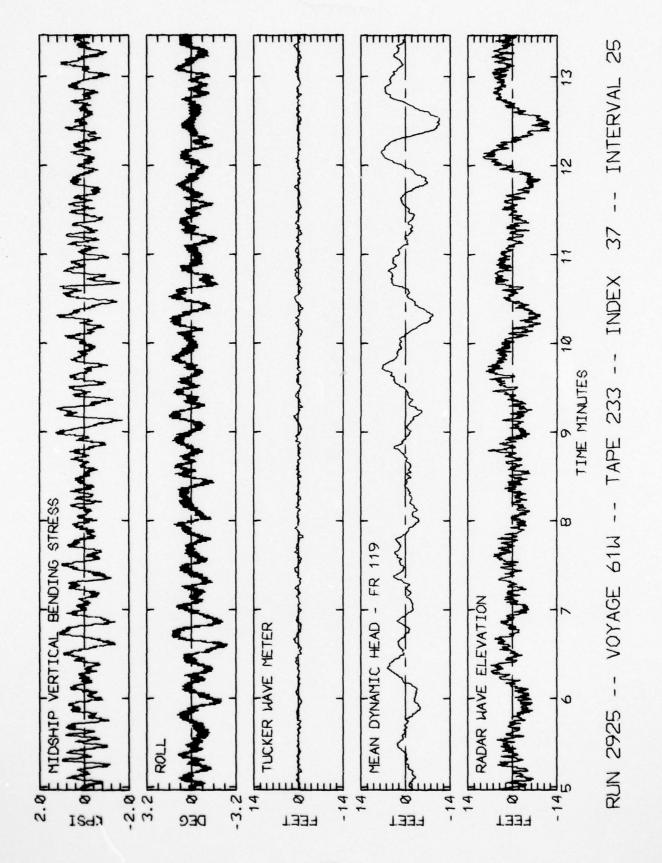
2 36 -- INTERVAL -- INDEX 233 -- TAPE VOYAGE 61W





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25 INTERVAL 37 --INDEX 233 --TAPE VOYAGE 61W RUN 2925 --



APPENDIX

THE DATA REDUCTION AND PRESENTATION PROCEDURE ACCORDING TO THE DEVELOPMENT IN REFERENCE 4

The data reduction procedure for each interval involved:

- a. Four main computation programs, the last one of which produced a complete file of results for each interval.
- b. Two lister programs to supply immediate indications of some of the results.
- c. One file consolidation program which produced one file for each voyage leg containing everything but the time histories of radar wave and mean dynamic head.
- d. Two programs to generate the final graphical presentations for each interval.

Items b through d amount to bookkeeping operations. The work was done in the four main computation programs.

The first computation program carried out the procedure described in Reference 4 for the radar. At its conclusion the radar wave spectrum and the computed time history were written in temporary files as was the time history of vertical displacement at the radar.

The second program involved reduction of the Tucker data. Both the original data and the displacement file produced by the first program were accessed. The procedure was carried out so that time histories of mean dynamic head and the Tucker Meter signal were available. These were spectrum analyzed, and all results written in a temporary file.

The third computation program accessed the various wave-related time histories (radar, Tucker, and mean dynamic head) and performed a peak-trough analysis on the middle 16-1/2 minutes of each. (Because of the tapering described in Reference 4 both the radar and mean dynamic head data are not valid for the first and last two minutes of sample.) The object of the peak-trough analysis was to produce double amplitude statistics. The zero crossing convention was used; that is, a crest was defined as the largest instantaneous value in an excursion above the sample mean, a trough was the smallest instantaneous value in an excursion below the sample mean. The double amplitude is the difference in elevation between crest and succeeding trough. In this approach small fluctuations are more or less ignored if they are riding on top of large ones. The results resemble the double amplitudes which would be estimated by hand from an oscillograph record except that the hand analyst would probably visually fair through superimposed noise whereas the computer does not. The effect is that while the computer gets about the same number of double amplitudes as the human analyst, the computer's answers tend to be higher if the records are noisy. From the double amplitudes found, the average of 1/3 and 1/10 highest were computed, and the position in the sample of the largest double amplitude was noted. All results, including the actual double amplitudes were written in a temporary file.

The fourth computation program accessed the original data and performed spectrum analyses upon the midship vertical bending stress and roll. It then accessed all previously written temporary files and produced a new file containing all of the results for the interval. These results included log-book data, results of the first analysis of raw data (Ref.3,5), five spectra along with all analysis parameters, all results from the peak-trough analysis, and the two new time histories, the radar wave and the mean dynamic head. These files were meant to be stored on magnetic tape for possible future reference.

The final presentation of results for each interval is contained on two charts. The first type of chart (which appears on the even numbered pages of this report) contains the scalar spectra and a tabulation of results. The second type of chart (odd numbered pages) involves sample time histories. Both are identified at the bottom with the DL run number, the voyage number, the analog tape and interval numbers, and the index number assigned by Teledyne.

Referring to any even page, the tabulation at the left is intended as a summary of the most significant numbers pertaining to the interval. At the top is as much of the original log-book data as it seemed reasonable to squeeze in. This includes date, time, position, and ship speed, as well as the visual estimates of wave and swell heights and directions. Directions are counted from the bow to port or starboard in degrees. The "sea state" is apparently the Beaufort wind. The final line in the first section of the tabulation includes comments on visual weather and, after the slash, any other comment appearing in the log.

The second box in the tabulation involves midship longitudinal stress results. Only two of the many numbers which are available could be included as indices. The first is the maximum peak to trough stress excursion as obtained in Reference 1 or 2. The second index is the significant stress (4 times rms) as derived from the area of the stress spectrum obtained in the present reduction.

The third box in the tabulation is a summary of motions. Again the "significant" motions (4 rms) are indicated. The value for roll was derived from spectrum area, that for pitch and accelerations from the rms of the basic data. (Unless there are significant linear trends in the data the differences are slight between "raw" and "spectrum" rms.) The last three items in the list involve various stages in the radar data reduction. The first is the slant range as recorded. The "vertical range is $R_{\rm c}(t)$ of the radar analysis. This entry is essentially the vertical component of the range relative to the position of the accelerometer package. The number was derived from the spectrum. The last entry is the significant displacement at the radar (significant doubly integrated acceleration). It too was derived from spectrum analyses.

In a sense, the table at the bottom of the tabulation contains the final numerical answers. Items in the first column pertain to the uncorrected Tucker Meter signal. The second column pertains to the mean dynamic

head developed in conjunction with the analysis of the Tucker meter, and the third column pertains to wave elevations derived from the radar system. The first row in the table is the number of double amplitudes found in the middle 16-1/2 minutes of the sample. Below this are noted the maximum height found and the averages of the 1/10 and 1/3 highest double amplitudes. The final line in the table is the significant (4 rms) height derived from the spectral analyses. Ordinarily it is expected that the last two lines of the table will be about the same.

At the right of any even page are plots of the five computed spectra. It was decided to standardize the frequency scale from 0 to 2 rad/sec. In the great majority of intervals everything of interest is contained in this range. In some intervals one spectrum or another is non-negligible beyond 2 rad/sec but nothing much has been seen beyond 2.5 rad/sec for any of the quantities analyzed except in the stress spectrum where something may often be noticed around the frequency of the first mode of vertical vibration. The folding frequency of the analyses is above 20 rad/sec; no aliasing is expected, Reference 3.

The stress and roll spectra are plotted together. The vertical scale is for the stress spectrum. The roll spectrum has been multiplied by the factor noted in the legend before plotting. Dimensions of the stress spectral density are (kpsi²/rad/sec) and those of the roll spectral density are (deg²/rad/sec).

All three wave related spectra (Tucker, mean dynamic head, and radar) are plotted together to the same scale. The dimension of the wave spectral density is (feet 2 /rad/sec). In the wave spectrum plot there is a vertical (slightly joggled) dashed line. This line marks the position of the low frequency cutoff, $\boldsymbol{\omega}_{o}$, discussed in Reference 4 in conjunction with double integration of the vertical accelerations. It is correct to interpret the position of this line as meaning that the double integration has been done correctly for higher frequencies, and incorrectly for lower frequencies.

There are several details about the spectrum analyses which are not documented in the plots because they are constant throughout the data reduction. First, the normalization of the spectra is such that the spectrum area equals variance. All spectra are derived from a Fast Fourier Transform analysis of an 8192 point sample. The fundamental results is 4096 spectral estimates of 2 degrees of freedom each. These estimates are uniformly spaced in frequency at a delta-frequency of 0.00511 rad/sec. In order to improve statistical reliability, the basic spectral estimates were averaged in blocks of 20 estimates at intervals of 10 estimates. The resulting averages are thus equi-speced on the frequency scale at intervals of $\Delta \omega = 0.0511$ rad/sec. This also means that adjacent spectral estimates as shown in the plot are not quite independent -- to about the same degree as spectral estimates from the older autocorrelation methods are not independent.

As a result of the averaging, each spectral estimate has 40 degrees of freedom associated with it. Accordingly, the 90% confidence bounds on the spectra shown in the charts may be formed by multiplying the values given by 0.72 and 1.51. Had the process sampled continued indefinitely and a large number of 20.5 minute samples been obtained and analyzed, nine out of ten of these new estimates of spectral density would be expected to lie within the bounds so constructed. The practical implication is simply that the influence of sampling variability upon the given numerical results is roughly the same as that associated with the result of most other full scale wave measurement exercises.

The last detail of the spectrum analysis is the "total degrees of freedom." This number is included in parentheses at the end of each line of legend because it depends upon the shape of each individual spectrum. It is an estimate of the proper number of degrees of freedom to use in constructing confidence bounds on the sample variance. If each of the numbers in the present 8192 point time histories had been picked randomly the "total degrees of freedom" would be 8191. This is not the case -- adjacent members of all the present time series are highly correlated so that the equivalent "random" sample size is much smaller. In the present data set the "total degrees of freedom" (TDF) is expected to vary between 60 and 600. Approximate 90% confidence bounds on the variances assuming a Normal zero mean process, may be constructed by multiplying the estimate by two factors derived from the percentage points of the Chi-square distribution. Examples of the values of these factors are given as follows:

TDF	Factor for Lower Bound	Factor for High Bound
60	.72	1.32
120	.80	1.27
200	.84	1.17
400	.89	1.12
600	.91	1.10

These are factors for the variances. The square root applies to the rms values so that very roughly the 90% confidence bounds on rms range from the sample rms \pm 15% for TDF = 60 to the sample rms \pm 5% for TDF = 600. The practical implications of these results are quite similar to those mentioned in connection with the confidence bounds on the spectra. There is only so much "precision" obtainable from one 20 minute sample of wave elevation -- that which was attacined in the present work appears comparable to that achieved in the past in similar studies. With respect to comparisons between wave meters or between data and predictions of rms ship responses there can be little justification to a concern about differences of 5 to 15% magnitude.

The sample time histories on the odd numbered pages need little explanation, except perhaps to say that the duration of the sample shown (8-1/2 minutes) was a compromise between a desire to display as much of

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RADAR AND TUCKER WAVEMETER DATA FROM SEA-LAND MCLEAN - VOYAGE 6--ETC(U)

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the 16-1/2 minutes of derived wave time histories as was possible in one page; and the desire to spread the time scale out so that individual fluctuations were visible for intervals involving high ship speed in head seas. To produce the charts an 8-1/2 minute portion of the available 16-1/2 minutes of sample was chosen such that the largest radar wave double amplitude is shown -- as well as (if possible) the largest mean dynamic head double amplitude.

It may be fairly asked why the effort in producing plotted time histories for each interval was considered worthwhile. The answer to the question is fairly simple. While the present data in its original analog form has been scanned systematically by eye, the process involved oscillograph records with a time scale of about 15 minutes to the inch. At this time compression only a gross idea of what was happening can be formed, no detailed assessment of the believability of the data can be made, and, most importantly, the odd malfunction which is enough to upset the spectrum estimates or the statistics may often go unnoticed. This last is considered most important in the radar data. It was pointed out in References 3 and 5 that an attempt was made to weed out intervals where the radar had evidently lost signal and re-established a new reference range. In this process only the most obvious instances could be identified; no guarantees could be made that all instances of moderate or small magnitude had been eliminated.

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	SIT-DL-77-1943
J. F. DALZELL	B 100024-74-C-5451
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It was the purpose of the present work to reduce this raw data, to develop and implement such corrections as were found necessary and feasible, and to correlate and evaluate the final results from the two wave meters. In carrying out this work it was necessary to at least partly reduce several other channels of recorded data, so that, as a by-product, reduced results were also obtained for midship bending stresses, roll, pitch, and two components of acceleration on the ship's bridge.

As the work progressed it became evident that the volume of documentation required would grow beyond the usual dimensions of a single technical report. For this reason the analyses, the methods, the detailed results, discussions, and conclusions are contained in a series of ten related reports.

This report is one of the six in the series in which the detailed results of the data reduction process are presented. Included in this report is the reduced data from the Third Season Voyage 61.

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